LT5579

## feATURES

- High Output IP3: +27.3dBm at 2.14GHz
- Low Noise Floor: $-158 \mathrm{dBm} / \mathrm{Hz}\left(\mathrm{P}_{\text {OUT }}=-5 \mathrm{dBm}\right)$

■ High Conversion Gain: 2.6dB at 2.14GHz
■ Wide Frequency Range: 1.5GHz to $3.8 \mathrm{GHz}^{*}$

- Low LO Leakage
- Single-Ended RF and LO

■ Low LO Drive Level: -1dBm

- Single 3.3V Supply
- $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ QFN24 Package


## APPLICATIONS

- GSM/EDGE, W-CDMA, UMTS, LTE and TD-SCDMA Basestations
- 2.6 GHz and 3.5 GHz WiMAX Basestations
- 2.4GHz ISM Band Transmitters
- High Performance Transmitters
*Operation over wider frequency range is possible with reduced performance.
Consult Linear Technology for information and assistance.


### 1.5 GHz to 3.8 GHz High Linearity nverting Mixer Upconverting Mixer

## DESCRIPTIOn

The $\mathrm{LT}^{\circledR} 5579$ mixer is a high performance upconverting mixer optimized for frequencies in the 1.5 GHz to 3.8 GHz range. The single-ended LO input and RF output ports simplify board layout and reduce system cost. The mixer needs only -1dBm of LO power and the balanced design results in low LO signal leakage to the RF output. At 2.6 GHz operation, the LT5579 provides high conversion gain of 1.3 dB , high OIP3 of +26 dBm and a low noise floor of $-157.5 \mathrm{dBm} / \mathrm{Hz}$ at a -5 dBm RF output signal level.

The LT5579 offers a high performance alternative to passive mixers. Unlike passive mixers, which have conversion Ioss and require high LO drive levels, the LT5579 delivers conversion gain at significantly lower LO input levels and is less sensitive to LO power level variations. The lower LO drive level requirements, combined with the excellent LO leakage performance, translate into lower LO signal contamination of the output signal.

## TYPICAL APPLICATION

Frequency Upconversion in 2.14GHz W-CDMA Transmitter


Gain, NF and OIP3 vs RF Output Frequency

ABSOLUTE MAXIMUM RATIOGS

## (Note 1)

Supply Voltage. ..... 4 V
LO Input Power ..... $+10 \mathrm{dBm}$
LO Input DC Voltage. .. ..... -0.3 V to $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$
RF Output DC Current ..... 60 mA
IF Input Power (Differential) ..... $+13 \mathrm{dBm}$
$\mathrm{IF}^{+}$, $\mathrm{IF}^{-}$DC Currents ..... 60mA
TJMAX ..... $150^{\circ} \mathrm{C}$
Operating Temperature Range ..... $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Storage Temperature Range $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$

## PIn CONFIGURATION



## ORDER INFORMATION

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING | PACKAGE DESCRIPTION | TEMPERATURE RANGE |
| :--- | :--- | :--- | :--- | :--- |
| LT5579IUH\#PBF | LT5579IUH\#TRPBF | 5579 | $24-$ Lead $(5 \mathrm{~mm} \times 5 \mathrm{~mm})$ Plastic QFN | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |

Consult LTC Marketing for parts specified with wider operating temperature ranges.
Consult LTC Marketing for information on non-standard lead based finish parts.
For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

## DC ELECTRICAL CHARACTERISTICS $V_{C C}=3.3 V_{,} \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ (Note 3), unless otherwise noted.

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power Supply Requirements (VCC) |  |  |  |  |  |
| Supply Voltage |  | 3.15 | 3.3 | 3.6 | $V_{D C}$ |
| Supply Current | $\begin{aligned} & V_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{P}_{\mathrm{LO}}=-1 \mathrm{dBm} \\ & \mathrm{~V}_{\mathrm{CC}}=3.6 \mathrm{~V}, \mathrm{P}_{\mathrm{LO}}=-1 \mathrm{dBm} \end{aligned}$ |  | $\begin{aligned} & 226 \\ & 241 \end{aligned}$ | 250 | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| Input Common Mode Voltage (V $\mathrm{V}_{\text {CM }}$ ) | Internally Regulated |  | 570 |  | mV |

## AC ELECTRICAL CHARACTERISTICS (Notes 2, 3)

| PARAMETER | CONDITIONS | MIN | TYP $\quad$ MAX |
| :--- | :--- | :---: | :---: | UNITS

AC ELECTRICAL CHARACTGRISTICS $V_{C C}=3.3 V, T_{A}=25^{\circ}, \mathrm{P}_{\text {If }}=-5 \mathrm{sibm}(-50 \mathrm{dBm} /$ /one for 2 -tone tests,
$\Delta f=1 \mathrm{MHz}), P_{\mathrm{Lo}}=-1 \mathrm{dBm}$, unless otherwise noted. Test circuits are shown in Figure 1. (Notes 2, 3)

| PARAMETER | CONDITIONS | MIN | TYP |
| :--- | :--- | :---: | :---: |
| IF Input Return Loss | $\mathrm{Z}_{0}=50 \Omega$, External Match | 15 | UNITS |
| LO Input Return Loss | $\mathrm{Z}_{0}=50 \Omega, 1100 \mathrm{MHz}$ to 4000MHz | dB |  |
| RF Output Return Loss | $\mathrm{Z}_{0}=50 \Omega$, External Match | $>9$ | dB |
| LO Input Power |  | -5 to 2 | dB |

$V_{C C}=3.3 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{PI}}=-5 \mathrm{dBm}(-5 \mathrm{dBm} /$ tone for 2-tone tests, $\Delta \mathrm{f}=1 \mathrm{MHz}), \mathrm{P}_{\mathrm{LO}}=-1 \mathrm{dBm}$, unless otherwise noted.
Low side LO for 1750MHz and 3600MHz. High side LO for 2140MHz and 2600MHz. (Notes 2, 3, 4)

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conversion Gain | $\begin{aligned} & \mathrm{f}_{\mathrm{fF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=45 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{array}{r} \hline 1.8 \\ 2.6 \\ 1.3 \\ -0.5 \end{array}$ |  | dB $d B$ $d B$ $d B$ |
| Conversion Gain vs Temperature $\left(T_{A}=-40^{\circ} \mathrm{C} \text { to } 85^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & f_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & f_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & f_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & -0.020 \\ & -0.020 \\ & -0.027 \\ & -0.027 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dB} /{ }^{\circ} \mathrm{C} \\ & \mathrm{~dB} /{ }^{\circ} \mathrm{C} \\ & \mathrm{~dB} /{ }^{\circ} \mathrm{C} \\ & \mathrm{~dB} /{ }^{\circ} \mathrm{C} \end{aligned}$ |
| Output 3rd Order Intercept | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=45 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{gathered} \hline 29 \\ 27.3 \\ 26.2 \\ 23.2 \end{gathered}$ |  | dBm <br> dBm <br> dBm <br> dBm |
| Output 2nd Order Intercept | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=45 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & 41 \\ & 42 \\ & 45 \\ & 54 \\ & \hline \end{aligned}$ |  | dBm dBm dBm dBm |
| Single Sideband Noise Figure | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{FF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & 9.2 \\ & 9.9 \\ & 12 \\ & 12 \\ & \hline \end{aligned}$ |  | dB dB dB dB |
| Output Noise Floor (Pout $=-5 \mathrm{dBm}$ ) | $\begin{aligned} & \mathrm{f}_{\mathrm{fF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{F}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & \hline-159.5 \\ & -158.1 \\ & -157.5 \\ & -155.5 \end{aligned}$ |  | $\mathrm{dBm} / \mathrm{Hz}$ $\mathrm{dBm} / \mathrm{Hz}$ $\mathrm{dBm} / \mathrm{Hz}$ $\mathrm{dBm} / \mathrm{Hz}$ |
| Output 1dB Compression | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{FF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & 13.3 \\ & 13.9 \\ & 13.7 \\ & 10.7 \end{aligned}$ |  | dBm <br> dBm <br> dBm <br> dBm |
| IF to LO Isolation | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHZ}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=45 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & 83 \\ & 81 \\ & 74 \\ & 73 \\ & \hline \end{aligned}$ |  | dB dB dB dB |
| LO to IF Leakage | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & f_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & f_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & -23 \\ & -28 \\ & -26 \\ & -22 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBm} \\ & \mathrm{dBm} \\ & \mathrm{dBm} \\ & \mathrm{dBm} \end{aligned}$ |
| LO to RF Leakage | $\begin{aligned} & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=1750 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2140 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=2600 \mathrm{MHz} \\ & \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{f}_{\mathrm{RF}}=3600 \mathrm{MHz} \end{aligned}$ |  | $\begin{aligned} & -39 \\ & -35 \\ & -36 \\ & -35 \end{aligned}$ |  | dBm <br> dBm <br> dBm <br> dBm |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.
Note 2: Each set of frequency conditions requires appropriate matching (see Figure 1).

Note 3: The LT5579 is guaranteed functional over the operating temperature range from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.
Note 4: SSB noise figure measurements performed with a small-signal noise source and bandpass filter on LO signal generator. No other IF signal applied.

# TYPICAL DC PERFORMANCE CHARACTERISTICS (Test Cirruit Shown in Figure 1) 



5579 G01

## TYPICAL AC PGRFORMANCE CHARACTERISTICS <br> 3300MHz to 3800MHz Application:

$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-5 \mathrm{dBm}\left(-5 \mathrm{dBm} /\right.$ tone for 2-tone tests, $\Delta \mathrm{f}=1 \mathrm{MHz}$ ), low side LO, $\mathrm{P}_{\mathrm{LO}}=-1 \mathrm{dBm}$, output measured at 3600 MHz , unless otherwise noted. (Test circuit shown in Figure 1)


Gain Distribution at 3600MHz

OIP3 Distribution at 3600MHz


5579 G03

SSB Noise Figure Distribution at 3600MHz


5579 G02

## TYPICAL AC PERFORMANCE CHARACTERISTICS 3300 mHzz to 3800mhz appication:

$V_{C C}=3.3 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-5 \mathrm{dBm}\left(-5 \mathrm{dBm} /\right.$ tone for 2 -tone tests, $\Delta \mathrm{f}=1 \mathrm{MHz}$ ), low side $\mathrm{LO}, \mathrm{P}_{\mathrm{L} 0}=-1 \mathrm{dBm}$, output measured at 3600 MHz , unless otherwise noted. (Test circuit shown in Figure 1)

## Conversion Gain and OIP3 vs RF Output Frequency



Conversion Gain and OIP3 vs LO Input Power


5579 G08
IM3 Level
vs RF Output Power (2-Tone)


5579 G11

## SSB Noise Figure <br> vs RF Output Frequency



5579 G06
SSB Noise Figure vs LO Input Power


5579 G09
IM2 Level
vs RF Output Power (2-Tone)


LO-RF Leakage vs RF Output Frequency


5579 G07
Conversion Gain and OIP3 vs Supply Voltage


## SSB Noise Figure

 vs Supply Voltage

## TYPICAL AC PGRFORMANCE CHARACTERISTICS <br> 2300MHz to 2700 MHz Application:

$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{\mathrm{IF}}=456 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-5 \mathrm{dBm}(-5 \mathrm{dBm} /$ tone for 2-tone tests, $\Delta \mathrm{f}=1 \mathrm{MHz})$, high side $\mathrm{LO}, \mathrm{P}_{\mathrm{L} 0}=-1 \mathrm{dBm}$, output measured at 2600 MHz , unless otherwise noted. (Test circuit shown in Figure 1)

Conversion Gain and OIP3
vs RF Output Frequency


5579 G14
Conversion Gain and OIP3 vs LO Input Power


5579 G17

SSB Noise Figure vs RF Output Frequency


5579 G15

## SSB Noise Figure <br> vs LO Input Power



IM2 Level vs RF Output Power (2-Tone)


LO-RF Leakage vs RF Output Frequency


5579 G16

## Conversion Gain and OIP3 vs Supply Voltage



SSB Noise Figure vs Supply Voltage


## TYPICAL PGRFORMANCE CHARACTGRISTICS 2100 MHz application:

$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-5 \mathrm{dBm}\left(-5 \mathrm{dBm} /\right.$ tone for 2 -tone tests, $\Delta \mathrm{f}=1 \mathrm{MHz}$ ), high side $\mathrm{LO}, \mathrm{P}_{\mathrm{LO}}=-1 \mathrm{dBm}$, output measured at 2140 MHz , unless otherwise noted. (Test circuit shown in Figure 1)

Conversion Gain and OIP3 vs RF Output Frequency


Conversion Gain and OIP3 vs LO Input Power


5579 G26
IM3 Level
vs RF Output Power (2-Tone)


5579 G29

SSB Noise Figure vs RF Output Frequency


5579 G24
SSB Noise Figure vs LO Input Power


5579 G27
IM2 Level
vs RF Output Power (2-Tone)


LO-RF Leakage vs RF Output Frequency


5579 G25
Conversion Gain and OIP3 vs Supply Voltage


5579 G19
SSB Noise Figure vs Supply Voltage


## TYPICAL PGRFORMAOCE CHARACTGRISTICS 1750MHz Appication:

$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{f}_{\mathrm{IF}}=240 \mathrm{MHz}, \mathrm{P}_{\mathrm{IF}}=-5 \mathrm{dBm}\left(-5 \mathrm{dBm} /\right.$ tone for 2 -tone tests, $\Delta \mathrm{f}=1 \mathrm{MHz}$ ), low side $\mathrm{LO}, \mathrm{P}_{\mathrm{LO}}=-1 \mathrm{dBm}$, output measured at 1750 MHz , unless otherwise noted. (Test circuit shown in Figure 1)

Conversion Gain and OIP3 vs RF Output Frequency


Conversion Gain and OIP3 vs LO Input Power


5579 G35

IM3 Level vs RF Output Power (2-Tone)


SSB Noise Figure vs RF Output Frequency


5579 G33

## SSB Noise Figure

vs LO Input Power


5579 G36
IM2 Level
vs RF Output Power (2-Tone)


LO-RF Leakage vs RF Output Frequency


5579 G34
Conversion Gain and OIP3 vs Supply Voltage


SSB Noise Figure vs Supply Voltage


## PIn functions

GND (Pins 1, 2, 5-7, 12-14, 16-18, 19-21, 23, 24): Ground Connections. These pins are internally connected to the exposed pad and should be soldered to a low impedance RF ground on the printed circuit board.
IF ${ }^{+}$, IF ${ }^{-}$(Pins 3, 4): Differential IF Input. The common mode voltage on these pins is set internally to 570 mV . The DC current from each pin is determined by the value of an external resistor to ground. The maximum DC current through each pin is 60 mA .
$V_{\text {CC }}$ (Pins 8-11): Power Supply Pins for the IC. These pins are connected together internally. Typical current consumption is 226 mA . These pins should be connected together on the circuit board with external bypass capacitors of 1000 pF , 100pF and 10 pF located as close to the pins as possible.

RF (Pin 15): Single-Ended RF Output. This pin is connected to an internal transformer winding. The opposite end of the winding is grounded internally. An impedance transformation may be required to match the output and a DC decoupling capacitor is required if the following stage has a DC bias voltage present.
LO (Pin22): Single-Ended Local Oscillator Input. An internal series capacitor acts as a DC block to this pin.

Exposed Pad (Pin 25): PGND. Electrical and thermal ground connection for the entire IC. This pad must be soldered to a low impedance RF ground on the printed circuit board. This ground must also provide a path for thermal dissipation.

## BLOCK DIAGRAM



## TEST CIRCUIT



| REF DES | $\begin{aligned} \mathrm{f}_{\mathrm{RF}} & =1750 \mathrm{MHz} \\ \mathrm{f}_{\mathrm{IF}} & =240 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} \mathrm{f}_{\mathrm{RF}} & =2140 \mathrm{MHz} \\ \mathrm{f}_{\mathrm{IF}} & =240 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} \mathrm{f}_{\mathrm{RF}} & =2600 \mathrm{MHz} \\ \mathrm{f}_{\mathrm{IF}} & =456 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} \mathrm{f}_{\mathrm{RF}} & =3600 \mathrm{MHz} \\ \mathrm{f}_{\mathrm{IF}} & =456 \mathrm{MHz} \end{aligned}$ | SIZE | COMMENTS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1, C2 | 82pF | 82pF | 33pF | 33pF | 0402 | AVX |
| C3 | - | - | 2.7pF | 1.8pF | 0402 | AVX |
| C4 | 100pF | 100pF | 100pF | 100pF | 0402 | AVX |
| C5 | 10pF | 10pF | 10pF | 10pF | 0603 | AVX |
| C6 | 1nF | 1 nF | 1 nF | 1nF | 0402 | AVX |
| C7 | $1 \mu \mathrm{~F}$ | $1 \mu \mathrm{~F}$ | $1 \mu \mathrm{~F}$ | $1 \mu \mathrm{~F}$ | 0603 | Taiyo Yuden LMK107BJ105MA |
| C8 | 1.2pF | 0.45pF | - | 0.7pF | 0402 | AVX ACCU-P |
| C9 | 33pF | 33pF | 33pF | 33pF | 0402 | AVX |
| L1, L2 | 40nH | 40nH | 40nH | 40nH | 0402 | Coilcraft 0402CS |
| L3 | 6.8 nH | 3.9 nH | 1 nH | $0 \Omega$ | 0402 | Toko LL1005-FHL/0』 Jumper |
| R1, R2 | 11 $\Omega$, 0.1\% | 11 $\Omega$, 0.1\% | 11 $\Omega$, 0.1\% | 11 $\Omega$, 0.1\% | 0603 | IRC PFC-W0603R-03-11R1-B |
| T1 | 4:1 | 4:1 | 4:1 | 4:1 | SM-22 | M/A-COM MABAES0061 |
| TL1, TL2* | - | - | 1 mm | 1.4 mm | - | $\mathrm{Z}_{0}=70 \Omega$ Microstrip |
| TL3 | 2 mm | 2 mm | 2 mm | 2 mm | - | $\mathrm{Z}_{0}=70 \Omega$ Microstrip |

*Center-to-center spacing between C9 and C3. Center of C9 is 2.6 mm from the edge of the IC package for all cases.

Figure 1. Test Circuit Schematic

## APPLICATIONS INFORMATION

The LT5579 uses a high performance LO buffer amplifier driving a double-balanced mixer core to achieve frequency conversion with high linearity. Internal baluns are used to provide single-ended LO input and RF output ports. The IF input is differential. The LT5579 is intended for operation in the 1.5 GHz to 3.8 GHz frequency range, though operation outside this range is possible with reduced performance.

## IF Input Interface

The IFinputs are tied to the emitters of the double-balanced mixer transistors, as shown in Figure 2. These pins are internally biased to a common mode voltage of 570 mV . The optimum DC current in the mixer core is approximately 50 mA per side, and is set by the external resistors, R1 and R2. The inductors and resistors must be able to handle the anticipated current and power dissipation. For best LO leakage performance the board layout must be symmetrical and the input resistors should be well matched ( $0.1 \%$ tolerance is recommended).

The purpose of the inductors (L1 and L2) is to reduce the loading effects of R1 and R2. The impedances of L1 and L2 should be at least several times greater than the IF input impedance at the desired IF frequency. The self-resonant frequency of the inductors should also be at least several times the IF frequency. Note that the DC resistances of L1 and L2 will affect the DC current and may need to be accounted for in the selection of R1 and R2.

L1 and L2 should connect to the signal lines as close to the package as possible. This location will be at the lowest impedance point, which will minimize the sensitivity of the performance to the loading of the shunt L-R branches.

Capacitors C1 and C2 are used to cancel out the parasitic series inductance of the IF transformer. They also provide DC isolation betweenthe IF ports to prevent unwanted interactions that can affect the LO to RF leakage performance.

The differential input resistance to the mixer is approximately $10 \Omega$, as indicated in Table 1. The package and external inductances (TL1 and TL2) are used along with


Figure 2. IF Input with External Matching

## APPLICATIONS INFORMATION

C 9 to step the impedance up to about $12.5 \Omega$. At lower frequencies additional series inductance may be required between the IF ports and C9. The position of C9 may vary with the IF frequency due to the different series inductance requirements. The 4:1 impedance ratio of transformer T1 completes the transformation to 50 ohms. Table 1 lists the differential IF input impedances and reflection coefficients for several frequencies.

Table 1. IF Input Differential Impedance

| FREQUENCY <br> (MHz) | IF INPUT <br> IMPEDANCE | REFLECTION COEFFICIENT |  |
| :---: | :---: | :---: | :---: |
|  |  | ANGLE |  |
| 70 | $8.8+j 1.3$ | 0.70 | 177 |
| 140 | $8.7+j 2.3$ | 0.70 | 175 |
| 170 | $9.0+j 2.8$ | 0.70 | 174 |
| 190 | $8.9+j 3.0$ | 0.70 | 173 |
| 240 | $9.0+j 4.0$ | 0.70 | 170 |
| 380 | $9.7+j 4.9$ | 0.68 | 168 |
| 450 | $10.0+j 5.2$ | 0.67 | 167 |
| 750 | $10.8+j 9.4$ | 0.65 | 158 |
| 1000 | $11.8+j 13.8$ | 0.64 | 148 |

The purpose of capacitor C3 is to improve the LO-RF leakage in some applications. This relatively small-valued capacitor has little effect on the impedance match in most cases. This capacitor should typically be located close to the IC, however, there may be cases where re-positioning the capacitor may improve performance.
The measured return loss of the IF input is shown in Figure 3 for application frequencies of $70 \mathrm{MHz}, 240 \mathrm{MHz}$ and 456MHz. Component values are listed in Table 2. (For 70MHz matching details, refer to Figure 8.)

Table 2. IF Input Component Values

| FREQUENCY <br> (MHz) | C1, C2 <br> (pF) | C9 <br> (pF) | C3 <br> (pF) | L1, L2 <br> (nH) | R1, R2 <br> ( $\mathbf{\Omega})$ | MATCH BW <br> (at 12dB RL) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $70(3)$ | 1000 | 120 | $(1)$ | 100 | 9.1 | $<50$ to 158 |
| 140 | 180 | 22 | $(1)$ | 100 | 9.1 | 112 to 170 |
| 240 | 82 | 33 | $(1)$ | 40 | 11 | 174 to 263 |
| 450 | 33 | 33 | $(1)$ | 40 | 11 | 330 to 505 |

Note: (1) Depends on RF, (2) T1 = M/A-Com MABAES0061,
(3) See Figure 8


5579 F03
Figure 3. IF Input Return Loss with 70MHz (a), 240MHz (b) and 456MHz (c) Matching

## APPLICATIONS INFORMATION

## LO Input Interface

The simplified schematic for the single-ended LO input port is shown in Figure 4. An internal transformer provides a broadband impedance match and performs single-ended to differential conversion. An internal capacitor also aids in impedance matching and provides DC isolation to the primary transformer winding. The transformer secondary feeds the differential limiting amplifier stages that drive the mixer core.

The measured return loss of the LO input port is shown in Figure 5 for an LO input power of -1 dBm . The impedance match is acceptable from about 1.1 GHz to beyond 4 GHz , with a minimum return loss across this range of about 9 dB at 2300 MHz . If desired, the return loss can be improved below 1.1 GHz by external components as shown in Figure 4. The return loss can also be improved by reducing the LO drive level, though performance will degrade if the level is too low.


Figure 4. LO Input Circuit

While external matching of the LO input is not required for frequencies above 1.1 GHz , external matching should be used for lower LO frequencies for best performance. Table 3 lists the input impedance and reflection coefficient vs frequency for the LO input for use in such cases.

Table 3. Single-Ended LO Input Impedance (at Pin 22, No External Match)

| FREQUENCY <br> (MHz) | INPUT <br> IMPEDANCE | REFLECTION COEFFICIENT |  |
| :---: | :---: | :---: | :---: |
|  |  | ANGLE |  |
| 750 | $63.3 \\|-\mathrm{j} 30.5$ | 0.68 | -125 |
| 1000 | $20.3 \\|-\mathrm{j} 1120$ | 0.42 | -179 |
| 1500 | $78.4 \\|-\mathrm{j} 1250$ | 0.22 | -7.7 |
| 1900 | $79.1\|\mid-\mathrm{j} 113$ | 0.34 | -65.2 |
| 2000 | $74.7 \\|-\mathrm{j} 96.3$ | 0.35 | -74.7 |
| 2150 | $66.8 \\|-\mathrm{j} 81.5$ | 0.36 | -87.0 |
| 2400 | $53.8 \\|-\mathrm{j} 69.8$ | 0.35 | -105 |
| 3050 | $33.7 \\|-\mathrm{j} 115$ | 0.26 | -148 |
| 3150 | $33.0 \\|-\mathrm{j} 146$ | 0.24 | -154 |
| 4000 | $43.9 \\|+\mathrm{j} 173$ | 0.15 | 123 |



Figure 5. LO Input Return Loss

## APPLICATIONS INFORMATION

## RF Output Interface

The RF output interface is shown in Figure 6. An internal RF transformer reduces the mixer core output impedance to simplify matching of the RF output pin. A center tap in the transformer provides the DC connection to the mixer core and the transformer provides DC isolation to the RF output. The RF pin is internally grounded through the secondary winding of the transformer, thus a DC voltage should not be applied to this pin.
While the LT5579 performs best at frequencies above 1500 MHz , the part can be used down to 900 MHz . The internal RF transformer is not optimized for these lower frequencies, thus the gain and impedance matching bandwidth will decrease due to the low transformer inductance. The impedance data for the RF output, listed in Table 4, can be used to develop matching networks for different frequencies or load impedances. Figure 7 illustrates the output return loss performance for several applications. The component values and approximate matching bandwidths are listed in Table 5.

## DC and RF Grounding

The LT5579 relies on the back side ground for both RF and thermal performance. The Exposed Pad must be soldered to the low impedance topside ground plane of the board. Several vias should connect the topside ground to other ground layers to aid in thermal dissipation.


Figure 6. RF Output Circuit

Table 4. Single-Ended RF Output Impedance (at Pin 15, No External Matching)

| FREQUENCY <br> (MHz) | RF OUTPUT <br> IMPEDANCE | REFLECTION COEFFICIENT |  |
| :---: | :---: | :---: | :---: |
|  |  | ANGLE |  |
| 1250 | $11.0+\mathrm{j} 42.7$ | 0.78 | 97.4 |
| 1750 | $55.6+\mathrm{j} 83.4$ | 0.62 | 47.8 |
| 1950 | $119+\mathrm{j} 62.4$ | 0.52 | 21.9 |
| 2150 | $116-\mathrm{j} 21.0$ | 0.42 | -10.4 |
| 2300 | $73.7-\mathrm{j} 37.7$ | 0.34 | -40.9 |
| 2600 | $35.2-\mathrm{j} 21.5$ | 0.30 | -110 |
| 3600 | $21.9+\mathrm{j} 17.8$ | 0.45 | 134 |

Table 5. RF Output Component Values

| FREQUENCY <br> (MHz) | C8 (pF) | L3 (nH) | MATCH BW (at 12dB RL) |
| :---: | :---: | :---: | :---: |
| 1650 | 1.5 | 6.8 | 1630 to 1770 |
| 1750 | 1.2 | 6.8 | 1725 to 1870 |
| 1950 | 1 | 4.7 | 1840 to 2020 |
| 2140 | 0.45 | 3.9 | 2035 to 2285 |
| 2600 | - | 1 | 2260 to $2780^{*}$ |
| 3600 | 0.7 | $0 \Omega$ | 3170 to $4100^{*}$ |

*10dB Return Loss bandwidth


Figure 7. RF Output Return Loss with 1750MHz (a), 2140 MHz (b), 2600 MHz (c) and 3600 MHz (d) Matching

## TYPICAL APPLICATIONS

The following examples illustrate the implementation and performance of the LT5579 in different frequency configurations. These circuits were evaluated using the circuit board shown in Figure 12.

## 1650MHz Application

In this case, the LT5579 was evaluated while tuned for an IF of 70 MHz and an RF output of 1650 MHz . The matching configuration is shown in Figure 8.

Input capacitors are used only as DC blocks in this application. The 4.7 nH inductors and the 120 pF capacitor transform the input impedance of the IC up to approximately


Figure 8. IF Input Tuned for 70MHz
$12.5 \Omega$. The relatively low input frequency demanded the use of 4.7 nH chip inductors instead of short transmission lines.

Closer to the IC input, 47pF capacitors were used instead of a single differential capacitor (C3 in Figure 1), because it was found that the addition of common mode capacitance improved the high side LO performance in this application. The value of these 47pF capacitors was selected to resonate with the 100 nH inductors at 70 MHz . Note that adding common mode capacitance does not improve performance with all frequency configurations.
The RF port impedance match was realized with C8 = 1.5 pF and $\mathrm{L} 3=6.8 \mathrm{nH}$. The optimum impedance match
was purposefully shifted high in order to achieve better OIP3 performance at the desired frequency.
Figure 9 shows the measured conversion gain and OIP3 as a function of RF output frequency. As mentioned above, the output impedance match is shifted towards the high side of the band, and this is evidenced by the positive slope of the gain. The single sideband noise figure across the frequency range is also shown.

Curves for both high side and low side LO cases are shown. In this particular application, the low side OIP3 outperforms the high side case.


Figure 9. Gain, Noise Figure and OIP3 vs RF Frequency with 70MHz IF and 1650MHz RF

## 1950MHz Application

In this example, a high side LO was used to convert the IF input signal at 240MHz to 1950MHz at the RF output. The RF port impedance match was realized with $\mathrm{C8}=1 \mathrm{pF}$ and $\mathrm{L} 3=4.7 \mathrm{nH}$. As in the 1650 MHz case, it was found that tuning the output match slightly high in frequency gave better OIP3 results at the desired frequency. The input match for 240 MHz operation is the same as described in the test circuit of Figure 1.
The measured 1950MHz performance is plotted in Figure 10 for both low side and high side LO drive. With this matching configuration, the low side LO case outperforms the high side LO. The gain, noise figure (SSB) and OIP3 are plotted as a function of RF output frequency.

## TYPICAL APPLICATIONS



5579 F10
Figure 10. Gain, Noise Figure and OIP3 vs RF Frequency for the 1950MHz Application

## 2140MHz with Low Side LO

The LT5579 was fully characterized with an RF output of 2140 MHz and a high side LO. The part also works well when driven with low side LO, however, the performance
benefited from the addition of common mode capacitance to the IF input match. A 10pF capacitor to ground was added to each IF pin. These capacitors were attached near inductors L1 and L2. The measured performance is shown in Figure 11.


Figure 11. Measured Performance when Tuned for 240MHz IF, 2140MHz RF and Low Side LO


Figure 12. LT5579 Evaluation Board (DC1233A)

## UH Package

24-Lead Plastic QFN ( $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1747 Rev A)


RECOMMENDED SOLDER PAD LAYOUT APPLY SOLDER MASK TO AREAS THAT ARE NOT SOLDERED


NOTE:

1. DRAWING IS NOT A JEDEC PACKAGE OUTLINE
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE

MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.20 mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION

ON THE TOP AND BOTTOM OF PACKAGE

## REVISION HISTORY

| REV | DATE | DESCRIPTION | PAGE NUMBER |
| :---: | :---: | :--- | :---: |
| A | $6 / 10$ | Revised Typical Application drawing. | 1 |
|  |  | Revised Absolute Maximum Ratings, Pin Configuration and DC Electrical Characteristics sections. | 2 |
|  |  | Revised AC Electrical Characteristics section parameters and Note 3. | 3 |
|  |  | Revised Figure 1 table. <br> Update Tables 2, 3 and 5 in Applications Information section <br> Added Typical Application drawing and graph, and revised Related Parts list | 11 |

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tion that the interconnection of its circuits as described herein will not infringe on existing patent rights.

## TYPICAL APPLICATION

## 2650MHz LTE Downlink Transmitter



## RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| Infrastructure |  |  |
| LT5527 | 400MHz to 3.7GHz, 5V Downconverting Mixer | 2.3dB Gain, 23.5dBm IIP3 and 12.5dB NF at 1900MHz, 5V/78mA Supply |
| LT5557 | 400MHz to 3.8GHz, 3.3V Downconverting Mixer | 2.9 dB Gain, 24.7dBm IIP3 and 11.7dB NF at 1950MHz, 3.3V/82mA Supply |
| LTC6400-X | 300MHz Low Distortion IF Amp/ADC Driver | Fixed Gain of $8 \mathrm{~dB}, 14 \mathrm{~dB}, 20 \mathrm{~dB}$ and 26 dB ; >36dBm OIP3 at 300 MHz , Differential I/0 |
| LTC6401-X | 140MHz Low Distortion IF Amp/ADC Driver | Fixed Gain of 8dB, 14dB, 20dB and 26dB; >40dBm OIP3 at 140MHz, Differential I/0 |
| LTC6416 | 2GHz 16-Bit ADC Buffer | 40.25 dBm OIP3 to 300MHz, Programmable Fast Recovery Output Clamping |
| LTC6412 | 31dB Linear Analog VGA | 35 dBm OIP3 at 240 MHz , Continuous Gain Range -14 dB to 17 dB |
| LT5554 | Ultralow Distort IF Digital VGA | 48 dBm OIP3 at 200MHz, 2dB to 18dB Gain Range, 0.125 dB Gain Steps |
| LT5575 | 700MHz to 2.7GHz Direct Conversion I/Q Demodulator | Integrated Baluns, 28dBm IIP3, 13dBm P1dB, 0.03dB I/Q Amplitude Match, $0.4^{\circ}$ Phase Match |
| LT5578 | 400MHz to 2.7GHz Upconverting Mixer | 27 dBm OIP3 at $900 \mathrm{MHz}, 24.2 \mathrm{dBm}$ at 1.95GHz, Integrated RF Transformer |
| LTC5598 | 5MHz to 1.6GHz I/Q Modulator | 27.7dBm OIP3 at 140MHz, 22.9dBm at 900MHz, -161.2dBm/Hz Noise Floor |
| RF Power Detectors |  |  |
| LT5534 | 50MHz to 3GHz Log RF Power Detector with 60dB Dynamic Range | $\pm 1 \mathrm{~dB}$ Output Variation over Temperature, 38ns Response Time, Log Linear Response |
| LT5537 | Wide Dynamic Range Log RF/IF Detector | Low Frequency to 1GHz, 83dB Log Linear Dynamic Range |
| LT5570 | 2.7GHz Mean-Squared Detector | $\pm 0.5 \mathrm{~dB}$ Accuracy Over Temperature and >50dB Dynamic Range, 500ns Rise Time |
| LT5581 | 6GHz Low Power RMS Detector | 40 dB Dynamic Range, $\pm 1 \mathrm{~dB}$ Accuracy Over Temperature, 1.5 mA Supply Current |
| ADCs |  |  |
| LTC2208 | 16-Bit, 130Msps ADC | 78dBFS Noise Floor, >83dB SFDR at 250MHz |
| LTC2262-14 | 14-Bit, 150Msps ADC Ultralow Power | 72.8dB SNR, 88dB SFDR, 149mW Power Consumption |
| LTC2242-12 | 12-Bit, 250Msps ADC | 65.4dB SNR, 78dB SFDR, 740mW Power Consumption |

