## General Description

The AAT4282A SmartSwitch ${ }^{\text {TM }}$ is a member of Skyworks' Application Specific Power MOSFET (ASPM ${ }^{\top M}$ ) product family. The AAT4282A is a dual P-channel MOSFET power switch designed for high-side load-switching applications. Each MOSFET has a typical $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}$ of $60 \mathrm{~m} \Omega$, allowing increased load switch current handling capacity with a low forward voltage drop. The device is available in three different versions with flexible turn-on and turn-off characteristics - from very fast to slew-rate limited. The standard 4282A (-1) version has a slew-rate limited turn-on load switch. The AAT4282A (-2) version features fast turn-on capability, typically less than 500ns turn-on and $3 \mu s$ turn-off times. The AAT4282A (-3) variation offers a shutdown load discharge circuit to rapidly turn off a load circuit when the switch is disabled. An additional feature is a slew-rate selector pin which can switch between fast and slow slew rate.

All the AAT4282A load switch versions are designed to operate from 1.5 V up to 6.5 V , making them ideal for both 3 V and 5 V systems. Input logic levels are TTL and 2.5 V to 5 V CMOS compatible. The quiescent supply current is a very low $1 \mu \mathrm{~A}$.

The AAT4282A is available in the Pb-free, low profile $2.0 \times 2.0 \mathrm{~mm}$ FTDFN22-8 package and the SC70JW-8 package and is specified over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ temperature range.

## Features

- $\mathrm{V}_{\mathrm{IN}}$ Range: 1.5 V to 6.5 V
- Low R ${ }_{\text {DS(ON) }}$
- 60m $\Omega$ Typical @ 5V
- 140m $\Omega$ Typical @ 1.5V
- Slew Rate Turn-On Time Options
- 1ms
- $0.5 \mu \mathrm{~s}$
- $100 \mu \mathrm{~s}$
- Fast Shutdown Load Discharge Option
- Low Quiescent Current
- Typically $1 \mu \mathrm{~A}$
- TTL/CMOS Input Logic Level
- Temperature Range $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
- FTDFN22-8 and SC70JW-8 Packages


## Applications

- Cellular Telephones
- Digital Still Cameras
- Hotswap Supplies
- Notebook Computers
- PDA Phones
- PDAs
- PMPs
- Smartphones


## Typical Application



## Slew Rate Controlled Load Switch

## Pin Descriptions

| Pin \# |  | Symbol | Function |
| :---: | :---: | :---: | :---: |
| FTDFN22-8 | SC70JW-8 |  |  |
| 1 | 8 | INA | This is the pin to the P-channel MOSFET source for Switch A. Bypass to ground through a $1 \mu \mathrm{~F}$ capacitor. INA is independent of INB |
| 2 | 7 | ENA | Active-High Enable Input A. A logic low turns the switch off and the device consumes less than $1 \mu \mathrm{~A}$ of current. Logic high resumes normal operation. |
| 3 | 6 | ENB | Active-High Enable Input B. A logic low turns the switch off and the device consumes less than $1 \mu \mathrm{~A}$ of current. Logic high resumes normal operation. |
| 4 | 5 | INB | This is the pin to the P-channel MOSFET source for Switch B. Bypass to ground through a $1 \mu \mathrm{~F}$ capacitor. INB is independent of INA. |
| 5 | 4 | OUTB | This is the pin to the P-channel MOSFET drain connection. Bypass to ground through a $0.1 \mu \mathrm{~F}$ capacitor. |
| 6 | 3 | GND | Ground connection |
| 7 | 2 | FAST | Active-high input Switches between FAST (Logic H) and SLOW (Logic L) Slew rate |
| 8 | 1 | OUTA | This is the pin to the P-channel MOSFET drain connection. Bypass to ground through a $0.1 \mu \mathrm{~F}$ capacitor. |

## Pin Configuration

FTDFN22-8
(Top View)


SC70JW-8
(Top View)


## Selector Guide

| Part Number | Slew Rate (Typ) |  |  | Enable |
| :---: | :---: | :---: | :---: | :---: |
|  | FAST (H) | SLOW (L) |  |  |
|  | 1 ms |  | NO | Active |
| AAT4282A-2 |  | NO | Active High |  |
| AAT4282A-3 | $0.5 \mu \mathrm{~s}$ |  | YES | Active High |

## Absolute Maximum Ratings ${ }^{2}$

| Symbol | Description | Value | Units |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | IN to GND | -0.3 to 7 | V |
| $\mathrm{~V}_{\text {EN }}$ FAST | EN, FAST to GND | -0.3 to 7 | V |
| $\mathrm{~V}_{\text {OUT }}$ | OUT to GND | -0.3 to $\mathrm{V}_{\text {IN }}+0.3$ | V |
| $\mathrm{I}_{\text {MAX }}$ | Maximum Continuous Switch Current | 3 | A |
| $\mathrm{I}_{\text {DM }}$ | Maximum Pulsed Current (Duty Cycle $\leq 10 \%$ ) | 5.5 | A |
| $\mathrm{~T}_{3}$ | Operating Junction Temperature Range | -40 to 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {LEAD }}$ | Maximum Soldering Temperature (at leads) | 300 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\text {ESD }}$ | ESD Rating ${ }^{3}-\mathrm{HBM}$ | 4000 | V |

## Thermal Characteristics ${ }^{4}$

| Symbol | Description | Value | Units |
| :---: | :--- | :---: | :---: |
| $\theta_{\text {JA }}$ | Thermal Resistance | 70 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{P}_{\mathrm{D}}$ | Maximum Power Dissipation | 1.78 | W |

[^0]
## Electrical Characteristics ${ }^{1}$

$\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40$ to $85^{\circ} \mathrm{C}$ unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. Per channel.

| Symbol | Description | Conditions | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AAT4282A All Versions |  |  |  |  |  |  |
| $\mathrm{V}_{\text {IN }}$ | Operation Voltage |  | 1.5 |  | 6.5 | V |
| $\mathrm{I}_{\mathrm{Q}}$ | Quiescent Current | ON/OFF $=$ ACTIVE, FAST $=\mathrm{V}_{\text {IN }}, \mathrm{I}_{\text {OUT }}=0$ |  |  | 1.0 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {(OFFF) }}$ | Off Supply Current | ON/OFF = Inactive, OUT = Open |  |  | 1.0 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {SD(OFF) }}$ | Off Switch Current | ON/OFF $=$ GND, $\mathrm{V}_{\text {OUT }}=0$ |  |  | 1.0 | $\mu \mathrm{A}$ |
| $\mathrm{R}_{\mathrm{DS} \text { (ON) }}$ | On-Resistance A or B | $\mathrm{V}_{\text {IN }}=6.5 \mathrm{~V}$ |  | 56 |  | $\mathrm{m} \Omega$ |
|  |  | $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$ |  | 60 | 130 |  |
|  |  | $\mathrm{V}_{\text {IN }}=4.2 \mathrm{~V}$ |  | 65 | 140 |  |
|  |  | $\mathrm{V}_{\text {IN }}=3.0 \mathrm{~V}$ |  | 76 | 160 |  |
|  |  | $\mathrm{V}_{\mathrm{IN}}=1.80 \mathrm{~V}$ |  | 110 | 230 |  |
|  |  | $\mathrm{V}_{\mathrm{IN}}=1.5 \mathrm{~V}$ |  | 140 | 280 |  |
| TCR ${ }_{\text {RDS }}$ | On Resistance Temperature Coefficient |  |  | 2800 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\text {IL }}$ | ON/OFF Input Logic Low Voltage | $\mathrm{V}_{\text {IN }}=1.5 \mathrm{~V}$ |  |  | 0.4 | V |
| $\mathrm{V}_{\mathrm{IH}}$ | ON/OFF Input Logic High Voltage | $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$ | 1.4 |  |  | V |
| $\mathrm{I}_{\text {SINK }}$ | ON/OFF Input Leakage | $\mathrm{V}_{\text {ON/OFF }}=5.5 \mathrm{~V}$ |  |  | 1.0 | $\mu \mathrm{A}$ |
| AAT4282A-1 ${ }^{\text {2 }}$ |  |  |  |  |  |  |
| $\mathrm{T}_{\mathrm{D} \text { (ON) }}$ | Output Turn-On Delay Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 20 | 40 | $\mu \mathrm{s}$ |
| $\mathrm{T}_{\text {ON }}$ | Turn-On Rise Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1000 | 1500 | $\mu \mathrm{s}$ |
| $\mathrm{T}_{\text {D(OFF) }}$ | Output Turn-OFF Delay Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 4.0 | 10 | $\mu \mathrm{s}$ |
| AAT4282A-2 ${ }^{\text {2 }}$ |  |  |  |  |  |  |
| $\mathrm{T}_{\mathrm{D} \text { (ON) }}$ | Output Turn-On Delay Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.5 | 2 | $\mu \mathrm{s}$ |
| $\mathrm{T}_{\text {on }}$ | Turn-On Rise Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 0.5 | 1.0 | $\mu \mathrm{s}$ |
| $\mathrm{T}_{\text {D(OFF) }}$ | Output Turn-OFF Delay Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 4.0 | 10 | $\mu \mathrm{s}$ |
| AAT4282A-3 |  |  |  |  |  |  |
| $\mathrm{T}_{\mathrm{D} \text { (ON) }}$ | Output Turn-On Delay Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 20 | 40 | $\mu \mathrm{s}$ |
| $\mathrm{T}_{\text {on }}$ | Turn-On Rise Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{FAST}=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 100 | 150 | $\mu \mathrm{s}$ |
| $\mathrm{T}_{\text {o }}$ | Turn-On Rise Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{FAST}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 1000 | 1500 | $\mu \mathrm{S}$ |
| $\mathrm{T}_{\text {D(OFF) }}$ | Output Turn-OFF Delay Time | $\mathrm{V}_{\text {IN }}=5 \mathrm{~V}, \mathrm{R}_{\text {LOAD }}=10 \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 4.0 | 10 | $\mu \mathrm{s}$ |
| $\mathrm{R}_{\text {PD }}$ | Output Pull-Down Resistance During OFF | ON/OFF $=$ Inactive, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 150 | 250 | $\Omega$ |

[^1]
## Typical Characteristics

$\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted.

Quiescent Current vs. Temperature
(No Load; Single Switch)


Off Supply Current vs. Temperature (No Load; EN = GND; VIN = 5V)


On-Resistance vs. Temperature


## Quiescent Current vs. Input Voltage <br> (No Load; Single Switch)



Typical ON/OFF Threshold vs. Input Voltage


On-Resistance vs. Input Voltage


## Typical Characteristics

$\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted.


Output Turn-On Delay Time

$$
\left(\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=10 \Omega\right)
$$



Time $(50 \mu \mathrm{~s} / \mathrm{div})$

## Output Turn-On <br> $\left(R_{L}=10 \Omega\right)$



Time (500 $\mu \mathrm{s} / \mathrm{div}$ )


Output Turn-On Delay Time $\left(V_{\text {IN }}=3 V ; R_{L}=20 \Omega\right)$


Time ( $50 \mu \mathrm{~s} / \mathrm{div}$ )


## Typical Characteristics

$\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ unless otherwise noted.


Time ( $5 \mu \mathrm{~s} / \mathrm{div}$ )

Output Turn-Off Delay Time $\left(\mathrm{V}_{\mathrm{IN}}=3 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=20 \Omega\right.$ )


Time ( $5 \mu \mathrm{~s} / \mathrm{div}$ )

Output Turn-Off Delay Time

$$
\left(\mathrm{V}_{\mathrm{IN}}=1.8 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=10 \Omega\right)
$$



Time ( $5 \mu \mathrm{~s} / \mathrm{div}$ )

## Functional Block Diagram



* AAT4282A-3 version only.


## Functional Description

The AAT4282A is a family of flexible dual P-channel MOSFET power switches designed for high-side load switching applications. There are three versions of the AAT4282A with different turn-on and turn-off characteristics to choose from, depending upon the specific requirements of an application. The first version, the AAT4282A-1, has a moderate turn-on slew rate feature, which reduces in-rush current when the MOSFET is turned on. This function allows the load switch to be implemented with either a small input capacitor or no input capacitor at all. During turn-on slewing, the current ramps linearly until it reaches the level required for the output load condition. The proprietary turn-on current control method works by careful control and monitoring of the MOSFET gate voltage. When the device is switched ON, the gate voltage is quickly increased to the threshold level of the MOSFET. Once at this level, the current begins to slew as the gate voltage is slowly increased until the MOSFET becomes fully enhanced. Once it has
reached this point the gate is quickly increased to the full input voltage and the $R_{D S(O N)}$ is minimized.
The second version, the AAT4282A-2, is a very fast switch intended for high-speed switching applications.

This version has no turn-on slew rate control and no special output discharge features. The final switch version, the AAT4282A-3, has the addition of a minimized slew rate limited turn-on function and a shutdown output discharge circuit to rapidly turn off a load when the load switch is disabled through the ON/OFF pin. Using the FAST input pin on the AAT4282A-3, the device can be manually switched to a slower slew rate.
All versions of the AAT4282A operate with input voltages ranging from 1.5 V to 6.5 V . All versions of this device have extremely low operating current, making them ideal for battery-powered applications.

The ON/OFF control pin is TTL compatible and will also function with 2.5 V to 5 V logic systems, making the AAT4282A an ideal level-shifting load switch.

Slew Rate Controlled Load Switch

## Applications Information

## Input Capacitor

A $1 \mu \mathrm{~F}$ or larger capacitor is typically recommended for $\mathrm{C}_{\text {IN }}$ in most applications. A $\mathrm{C}_{\text {IN }}$ capacitor is not required for basic operation; however, it is useful in preventing load transients from affecting upstream circuits. $\mathrm{C}_{\mathrm{IN}}$ should be located as close to the device VIN pin as practically possible. Ceramic, tantalum, or aluminum electrolytic capacitors may be selected for $\mathrm{C}_{\mathrm{IN}}$. There is no specific capacitor equivalent series resistance (ESR) requirement for $\mathrm{C}_{\mathrm{IN}}$. However, for higher current operation, ceramic capacitors are recommended for $\mathrm{C}_{\text {IN }}$ due to their inherent capability over tantalum capacitors to withstand input current surges from low-impedance sources, such as batteries in portable devices.

## Output Capacitor

For proper slew operation, a $0.1 \mu \mathrm{~F}$ capacitor or greater is required between VOUT and GND. Likewise, with the output capacitor, there is no specific capacitor ESR requirement. If desired, $\mathrm{C}_{\text {out }}$ may be increased without limit to accommodate any load transient condition without adversely affecting the slew rate.

## Enable Function

The AAT4282A features an enable / disable function. This pin (ON) is active high and is compatible with TLL or CMOS logic. To assure the load switch will turn on, the ON control level must be greater than 1.4 V . The load switch will go into shutdown mode when the voltage on the ON pin falls below 0.4 V . When the load switch is in shutdown mode, the OUT pin is tri-stated, and quiescent current drops to leakage levels below $1 \mu \mathrm{~A}$.

## Reverse Output-to-Input Voltage Conditions and Protection

Under normal operating conditions, a parasitic diode exists between the output and input of the load switch. The input voltage should always remain greater than the output load voltage, maintaining a reverse bias on the internal parasitic diode. Conditions where $\mathrm{V}_{\text {out }}$ might exceed $\bigvee_{\text {IN }}$ should be avoided since this would forward bias the internal parasitic diode and allow excessive cur-
rent flow into the VOUT pin, possibly damaging the load switch. In applications where there is a possibility of $\mathrm{V}_{\text {out }}$ exceeding $\mathrm{V}_{\text {IN }}$ for brief periods of time during normal operation, the use of a larger value $\mathrm{C}_{\mathrm{IN}}$ capacitor is highly recommended. A larger value of $\mathrm{C}_{\mathrm{IN}}$ with respect to $\mathrm{C}_{\text {out }}$ will effect a slower $\mathrm{C}_{\text {IN }}$ decay rate during shutdown, thus preventing $\mathrm{V}_{\text {out }}$ from exceeding $\mathrm{V}_{\mathrm{IN}}$. In applications where there is a greater danger of $\mathrm{V}_{\text {out }}$ exceeding $\mathrm{V}_{\text {IN }}$ for extended periods of time, it is recommended to place a Schottky diode from $\mathrm{V}_{\text {IN }}$ to $\mathrm{V}_{\text {OUT }}$ (connecting the cathode to $\mathrm{V}_{\mathrm{IN}}$ and anode to $\mathrm{V}_{\text {Out }}$ ). The Schottky diode forward voltage should be less than 0.45 V .

## Thermal Considerations and High Output Current Applications

The AAT4282A is designed to deliver a continuous output load current. The limiting characteristic for maximum safe operating output load current is package power dissipation. In order to obtain high operating currents, careful device layout and circuit operating conditions must be taken into account.

The following discussions will assume the load switch is mounted on a printed circuit board utilizing the minimum recommended footprint as stated in the Printed Circuit Board Layout Recommendations section of this datasheet.
At any given ambient temperature $\left(T_{A}\right)$, the maximum package power dissipation can be determined by the following equation:

$$
P_{D(M A X)}=\frac{T_{J M A X)}-T_{A}}{\theta_{J A}}
$$

Constants for the AAT4282A are maximum junction temperature $\left(\mathrm{T}_{\mathrm{J} \text { (MAX) }}=125^{\circ} \mathrm{C}\right)^{1}$ and package thermal resistance ( $\theta_{\mathrm{JA}}=70^{\circ} \mathrm{C} / \mathrm{W}$ ). Worst case conditions are calculated at the maximum operating temperature, $\mathrm{T}_{\mathrm{A}}=$ $85^{\circ} \mathrm{C}$. Typical conditions are calculated under normal ambient conditions where $T_{A}=25^{\circ} \mathrm{C}$. At $\mathrm{T}_{\mathrm{A}}=85^{\circ} \mathrm{C}$, $\mathrm{P}_{\mathrm{D} \text { (MAX })}=571 \mathrm{~mW}$. At $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{D} \text { (MAX) }}=1429 \mathrm{~mW}$.
The maximum continuous output current for the AAT4282A is a function of the package power dissipation and the $R_{D S}$ of the MOSFET at $T_{J \text { (MAX) }}$. The maximum $R_{D S}$ of the MOSFET at $\mathrm{T}_{\text {JMAX) }}$ is calculated by increasing the

[^2]maximum room temperature $\mathrm{R}_{\mathrm{DS}}$ by the $\mathrm{R}_{\mathrm{DS}}$ temperature coefficient. The temperature coefficient $\left(T_{C}\right)$ is $2800 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. Therefore, at $125^{\circ} \mathrm{C}$ :
$R_{D S(\text { MAX })}=R_{D S\left(25^{\circ} \mathrm{C}\right)} \cdot\left(1+\mathrm{T}_{\mathrm{C}} \cdot \Delta \mathrm{T}\right) \Omega$
$\left.R_{\text {DS(MAX) }}=130 \mathrm{~m} \Omega \cdot+0.002800 \cdot\left(125^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right)\right)$
$R_{\text {DS(MAX) }}=166.4 \mathrm{~m} \Omega$
For maximum current, refer to the following equation:
$$
\mathrm{I}_{\mathrm{OUT}(\mathrm{MAX})}<\sqrt{\frac{\mathrm{P}_{\mathrm{D}(\mathrm{MAX})}}{\mathrm{R}_{\mathrm{DS}}}}
$$

For example, if $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}, \mathrm{R}_{\mathrm{DS}(\text { MAX })}=166.4 \mathrm{~m} \Omega$, and $\mathrm{T}_{\mathrm{A}}=$ $25^{\circ} \mathrm{C}, \mathrm{I}_{\text {OUt(MAX) }}=2.93 \mathrm{~A}$. If the output load current were to exceed 2.93 A or if the ambient temperature were to increase, the internal die temperature would increase and the device would be damaged. Higher peak currents can be obtained with the AAT4282A. To accomplish this, the device thermal resistance must be reduced by increasing the heat sink area or by operating the load switch in a duty cycle manner. Duty cycles with peaks less than 2 ms in duration can be considered using the method described in the High Peak Current Applications section of this datasheet.

## High Peak Output Current Applications

Some applications require the load switch to operate at a continuous nominal current level with short duration, high-current peaks. Refer to the $\mathrm{I}_{\mathrm{DM}}$ specification in the Absolute Maximum Ratings table to ensure the AAT4282A's maximum pulsed current rating is not exceeded. The duty cycle for both output current levels must be taken into account. To do so, first calculate the power dissipation at the nominal continuous current level, and then add the additional power dissipation due to the short duration, high-current peak scaled by the duty factor. For example, a $4 V$ system using an AAT4282A which has channel A operates at a continuous 1A load current level, and channel B operates at a continuous 100 mA load current level and has short 3A current peaks, as in a GSM application. The current peak occurs for $576 \mu$ s out of a 4.61 ms period. First, the current duty cycle is calculated:

$$
\begin{aligned}
& \% \text { Peak Duty Cycle }=\frac{x}{100}=\frac{576 \mu \mathrm{~s}}{4.61 \mathrm{~ms}} \\
& \% \text { Peak Duty Cycle }=12.5 \%
\end{aligned}
$$

The load current is 100 mA for $87.5 \%$ of the 4.61 ms period and 3 A for $12.5 \%$ of the period. Since the

Electrical Characteristics do not report $\mathrm{R}_{\mathrm{DS}(\mathrm{MAX})}$ for 4 V operation, it must be approximated by consulting the chart of $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})} \mathrm{vs}$. $\mathrm{V}_{\mathrm{IN}}$. The $\mathrm{R}_{\mathrm{DS}}$ reported for 5 V at 100 mA and 3A can be scaled by the ratio seen in the chart to derive the $R_{D S}$ for $4 V V_{\text {IN }}$ at $25^{\circ} \mathrm{C}: 130 \mathrm{~m} \Omega \cdot 63 \mathrm{~m} \Omega / 60 \mathrm{~m} \Omega$ $=136.5 \mathrm{~m} \Omega$. De-rated for temperature: $136.5 \mathrm{~m} \Omega \cdot(1+$ $\left.0.002800 \cdot\left(125^{\circ} \mathrm{C}-25^{\circ} \mathrm{C}\right)\right)=174.7 \mathrm{~m} \Omega$.

For channel A, the power dissipation for a continuous 1 A load is calculated as follows:
$P_{\mathrm{D}(\mathrm{CHA})}=\mathrm{I}_{\mathrm{OUT}}{ }^{2} \cdot \mathrm{R}_{\mathrm{DS}}=(1 \mathrm{~A})^{2} \cdot 174.7 \mathrm{~m} \Omega=174.7 \mathrm{~mW}$
For channel $B$, the power dissipation for 100 mA load is calculated as follows:
$P_{D(M A X)}=I_{\text {OUT }}{ }^{2} \cdot R_{D S}$
$P_{D(100 m A)}=(100 \mathrm{~mA})^{2} \cdot 174.7 \mathrm{~m} \Omega$
$P_{D(100 \mathrm{~mA})}=1.75 \mathrm{~mW}$
$P_{D(87.5 \% \mathrm{D} / \mathrm{C})}=\% \mathrm{DC} \cdot \mathrm{P}_{\mathrm{D}(100 \mathrm{~mA})}$
$P_{D(87.5 \% D / C)}=0.875 \cdot 1.75 \mathrm{~mW}$
$P_{D(87.5 \% \mathrm{D} / \mathrm{C})}=1.53 \mathrm{~mW}$
The power dissipation for 100 mA load at $87.5 \%$ duty cycle is 1.53 mW . Now the power dissipation for the remaining $12.5 \%$ of the duty cycle at 3 A is calculated:
$P_{D(M A X)}=I_{\text {OUT }}{ }^{2} \cdot R_{D S}$
$P_{D(3 A)}=(3 A)^{2} \cdot 174.7 \mathrm{~m} \Omega$
$P_{D(3 A)}=1572 \mathrm{~mW}$
$P_{D(12.5 \% \mathrm{D} / \mathrm{C})}=\% \mathrm{DC} \cdot \mathrm{P}_{\mathrm{D}(3 \mathrm{~A})}$
$P_{D(12.5 \% \mathrm{D} / \mathrm{C})}=0.125 \cdot 1572 \mathrm{~mW}$
$P_{\mathrm{D}(12.5 \% \mathrm{D} / \mathrm{C})}=196.7 \mathrm{~mW}$
Finally, the total power dissipation for channels $A$ and $B$ is determined as follows:
$P_{D(\text { total })}=P_{D(C H A)}+P_{D(100 m A)}+P_{D(3 A)}$
$P_{D \text { (total) }}=174.7 \mathrm{~mW}+1.53 \mathrm{~mW}+196.7 \mathrm{~mW}$
$P_{D \text { (total) }}=373 \mathrm{~mW}$
The maximum power dissipation for the AAT4282A operating at an ambient temperature of $85^{\circ} \mathrm{C}$ is 373 mW . The device in this example will have a total power dissipation of 571 mW . This is well within the thermal limits for safe operation of the device; in fact, at $85^{\circ} \mathrm{C}$, the AAT4282A will handle a 3 A pulse for up to $25 \%$ duty cycle. At lower ambient temperatures, the duty cycle can be further increased.

## Printed Circuit Board Layout Recommendations

For proper thermal management, and to take advantage of the low $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}$ of the AAT4282A, a few circuit board layout rules should be followed: $\mathrm{V}_{\text {IN }}$ and $\mathrm{V}_{\text {OUt }}$ should be routed using wider than normal traces, and GND should be connected to a ground plane. For best performance, $\mathrm{C}_{\text {IN }}$ and $\mathrm{C}_{\text {out }}$ should be placed close to the package pins.

## Evaluation Board Layout

The AAT4282A evaluation layout follows the printed circuit board layout recommendations and can be used for good applications layout. Refer to Figures 1 through 6.

Note: Board layout shown is not to scale.


C1, C2 1 $\mu \mathrm{F} 0603$ X5R 10V (P/N: GRM188R61A105KA61D)
C3, C4 $0.1 \mu \mathrm{~F} 0603$ X5R 10V (P/N: GRM188R71C104KA01D)
Figure 1: AAT4282AIPS Evaluation Board Schematic.


Figure 2: AAT4282AIPS Evaluation Board Top Side Layout.


Figure 3: AAT4282AIPS Evaluation Board Bottom Side Layout.


C1, C2 1 $\mu \mathrm{F} 0603$ X5R 10 V (P/N: GRM188R61A105KA61D)
C3, C4 0.1 $\mu \mathrm{F} 0603$ X5R 10V (P/N: GRM188R71C104KA01D)
Figure 4: AAT4282AIFS Evaluation Board Schematic.


Figure 5: AAT4282AIFS Evaluation Board Top Side Layout.


Figure 6: AAT4282AIFS Evaluation Board Bottom Side Layout.

## Ordering Information

| Device Option | Package | Marking $^{1}$ | Part Number (Tape and Reel) ${ }^{2}$ |
| :---: | :---: | :---: | :---: |
| AAT4282A-3 | FTDFN22-8 | WKXYY | AAT4282AIPS-3-T1 |
| AAT4282A-3 | SC70JW-8 | A8XYY | AAT4282AIFS-3-T1 |

Skyworks Green ${ }^{\text {TM }}$ products are compliant with
all applicable legislation and are halogen-free.
For additional information, refer to Skyworks
Definition of Green ${ }^{T M}$, document number
SQ04-0074.

## Package Information ${ }^{3}$

FTDFN22-8


Side View


All dimensions in millimeters.

1. $X Y Y=$ assembly and date code.
2. Sample stock is generally held on part numbers listed in BOLD.
 ing process. A solder fillet at the exposed copper edge cannot be guaranteed and is not required to ensure a proper bottom solder connection.

## SC70JW-8



All dimensions in millimeters.

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[^0]:    1. Parts not available in stock, but can be ordered.
     specified is not implied. Only one Absolute Maximum Rating should be applied at any one time
    2. Human body model is a 100 pF capacitor discharged through a $1.5 \mathrm{k} \Omega$ resistor into each pin.
    3. Mounted on a AAT4282A demo board in still $25^{\circ} \mathrm{C}$ air.
[^1]:     relation with statistical process controls.
    2. Contact factory for other turn on and delay options.

[^2]:     ity of over-temperature damage.

