

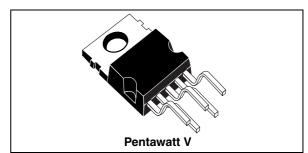
20-watt hi-fi audio power amplifier

Features

- Wide-range supply voltage, up to 40 V
- Single or split power supply
- Short-circuit protection to ground
- Thermal shutdown

Description

The TDA2040 is a monolithic integrated circuit in the Pentawatt package, intended for use as an audio class-AB amplifier. Typically, it provides 22 W output power into 4 Ω with THD = 0.5% at Vs = 32 V. The TDA2040 provides high output current and has very low harmonic and crossover distortion. Furthermore, the device incorporates a patented short-circuit protection system comprising an arrangement for automatically

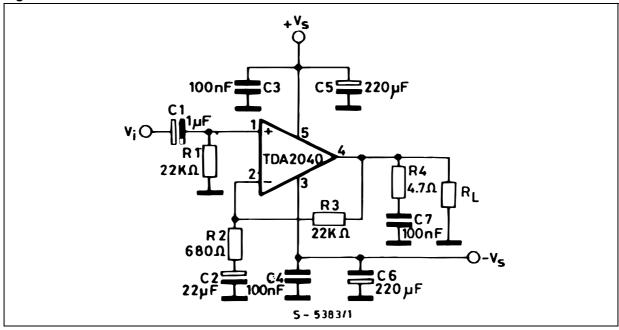


limiting the dissipated power so as to keep the operating point of the output transistors within their safe operating range. A thermal shutdown system is also included.

Table 1. Device summary

| Order code | Package |
|------------|------------------------|
| TDA2040V | Pentawatt V (vertical) |

Figure 1. TDA2040 test circuit



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Pin connections TDA2040

1 Pin connections

Figure 2. Schematic diagram

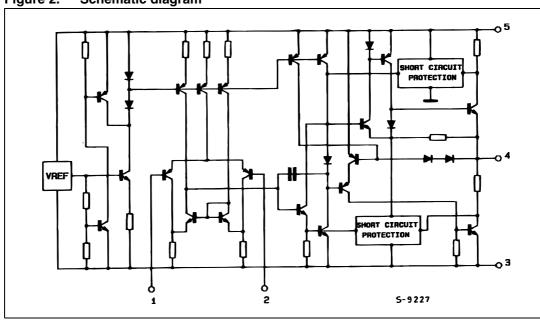
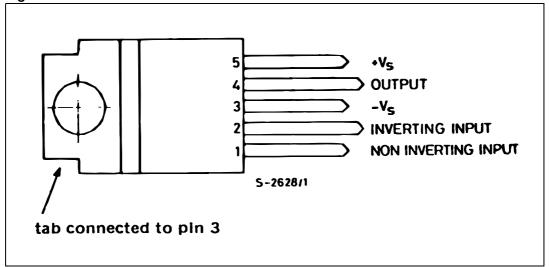


Figure 3. Pin connections



2 Electrical specifications

2.1 Absolute maximum ratings

Table 2. Absolute maximum ratings

| Symbol | Parameter | Value | Unit |
|-----------------------------------|---|------------|------|
| Vs | Supply voltage | ±20 | ٧ |
| Vi | Input voltage | Vs | |
| Vi | Differential input voltage | ±15 | ٧ |
| lo | Output peak current (internally limited) | 4 | Α |
| P _{tot} | Power dissipation at Tcase = 75 °C | 25 | W |
| T _{stg} , T _j | Storage and junction temperature | -40 to 150 | °C |
| V _{ESD_HBM} | ESD maximum withstanding voltage range, test condition CDF-AEC-Q100-002- "Human body model" | ±1500 | V |

2.2 Thermal data

Table 3. Thermal data

| Symbol | Parameter | | Тур | Max | Unit |
|------------------------|-------------------------------------|--|-----|-----|------|
| R _{th_j-case} | Thermal resistance junction to case | | - | 3 | °C/W |

2.3 Electrical characteristics

The specifications given here were obtained with the conditions $V_S = \pm 16$ V, $T_{amb} = 25$ °C unless otherwise specified.

Table 4. Electrical characteristics

| Symbol | Parameter | Test conditions | Min | Тур | Max | Unit |
|-----------------|-------------------------|---|------|---------|-----------|----------|
| V_S | Supply voltage | - | ±4.5 | - | ±20 | V |
| I _d | Quiescent drain current | $V_S = \pm 4.5 \text{ V}$ $V_S = \pm 20 \text{ V}$ | - | - 45 | 30 100 | mA mA |
| I _b | Input bias current | V _S = ±20 V | - | 0.3 | 1 | μΑ |
| V _{OS} | Input offset voltage | V _S = ±20 V | - | ±2 | ±20 | mV |
| Ios | Input offset current | - | - | | ±200 | nA |

Table 4. Electrical characteristics (continued)

| Symbol | Parameter | Test conditions | Min | Тур | Max | Unit |
|------------------|---------------------------------------|--|------|----------|----------|------|
| Po | Output power | $d = 0.5\%, f = 1 \text{ kHz},$ $T_{amb} = 60 \text{ °C}$ $R_L = 4 \Omega$ $R_L = 8 \Omega$ | 20 | 22 12 | - | w |
| | | d = 0.5%, f = 15 kHz; $T_{amb} = 60 \text{ °C}$ $R_L = 4 \Omega$ | 15 | 18 | - | |
| BW | Power bandwidth | $P_0 = 1 \text{ W}, R_L = 4 \Omega$ | - | 100 | - | Hz |
| G _{vOL} | Voltage gain (open loop) | f = 1 kHz | - | 80 | - | dB |
| G _v | Voltage gain (closed loop) | f = 1 kHz | 29.5 | 30 | 30.5 | dB |
| d Total harmon | Total harmonic distortion | $P_{o} = 0.1 \text{ to } 10 \text{ W},$ $R_{L} = 4 \Omega,$ $f = 40 \text{ to } 15000 \text{ Hz}$ | - | 0.08 | - | % |
| | | $P_0 = 0.1 \text{ to } 10 \text{ W},$ $R_L = 4 \Omega, f = 1 \text{ kHz}$ | - | 0.03 | - | % |
| e _N | Input noise voltage | B = Curve A B = 22 Hz to 22 kHz | - | 2 | - 10 | μV |
| I _N | Input noise current | B = Curve A B = 22 Hz to 22 kHz | - | 50 80 | - 200 | рА |
| R _i | Input resistance (pin 1) | - | 0.5 | 5 | - | ΜΩ |
| SVRR | Supply voltage rejection ratio | $\begin{aligned} G_V &= 30 \text{ dB, } R_L = 4 \Omega, \\ R_g &= 22 \text{ k}\Omega, \text{ f} = 100 \text{ Hz} \\ V_{ripple} &= 0.5 \text{ V RMS} \end{aligned}$ | 40 | 50 | - | dB |
| h | Efficiency | $f = 1 \text{ kHz} \\ P_0 = 12 \text{ W}, R_L = 8 \Omega \\ P_0 = 22 \text{ W}, R_L = 4 \Omega$ | - | 66 63 | - | % |
| T _j | Thermal shutdown junction temperature | - | - | - | 145 | °C |

2.4 Characterizations

Figure 4. Output power vs. supply voltage

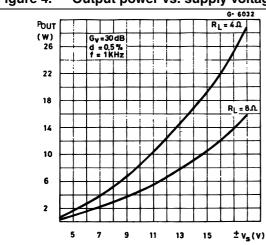


Figure 5. Output power vs. supply voltage

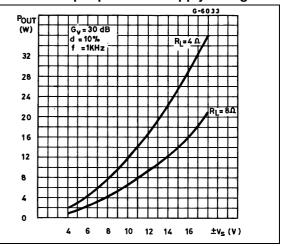


Figure 6. Output power vs. supply voltage

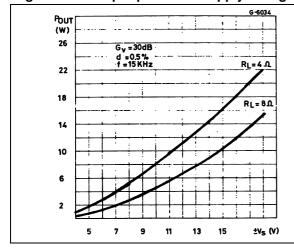


Figure 7. Distortion vs. frequency

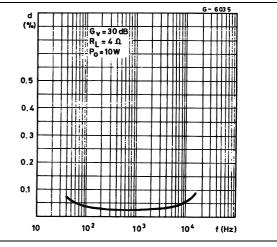


Figure 8. SVRR vs. frequency

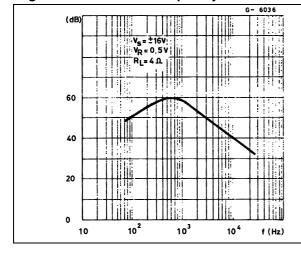
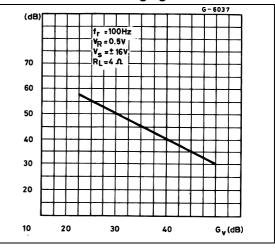


Figure 9. SVRR vs. voltage gain



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f (Hz)

Figure 10. Quiescent drain current vs. supply Figure 11. Open loop gain vs. frequency voltage

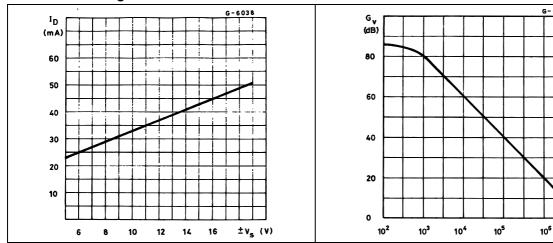
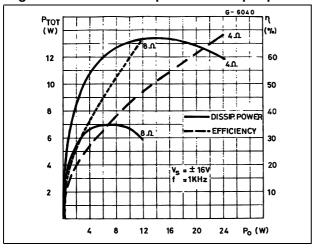


Figure 12. Power dissipation vs. output power



3 Applications

3.1 Circuits and PCB layout

Figure 13. Amplifier with split power supply

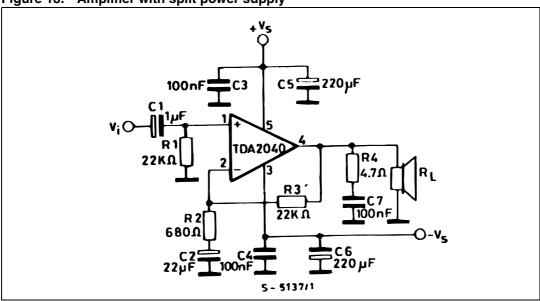
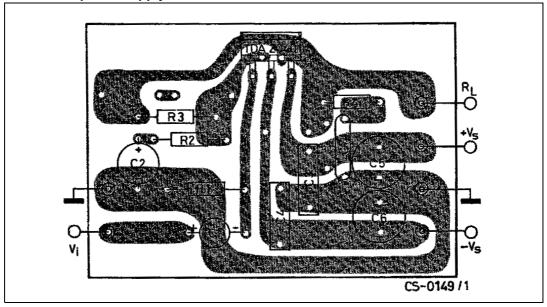


Figure 14. PCB and components layout for the circuit of the amplifier with split power supply



Applications TDA2040

Figure 15. Amplifier with single power supply

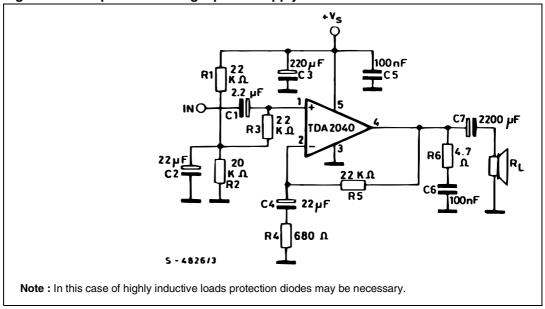


Figure 16. PCB and components layout for the circuit of the amplifier with single power supply

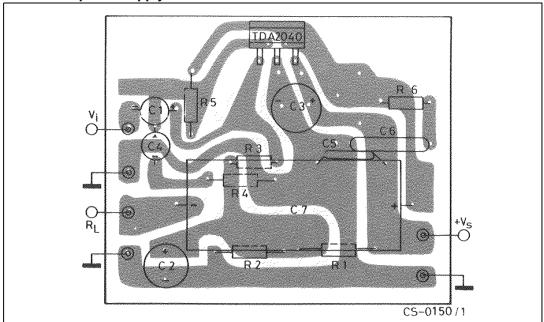
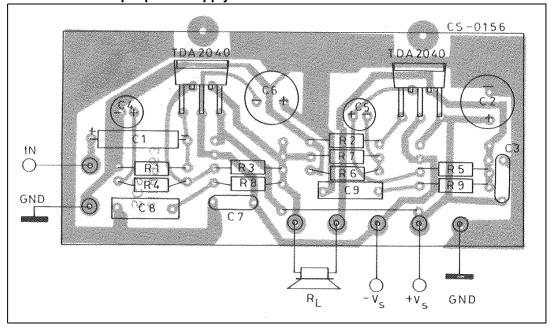


Figure 17. 30-watt bridge amplifier with split power supply

Figure 18. PCB and components layout for the circuit of the 30-watt bridge amplifier with split power supply



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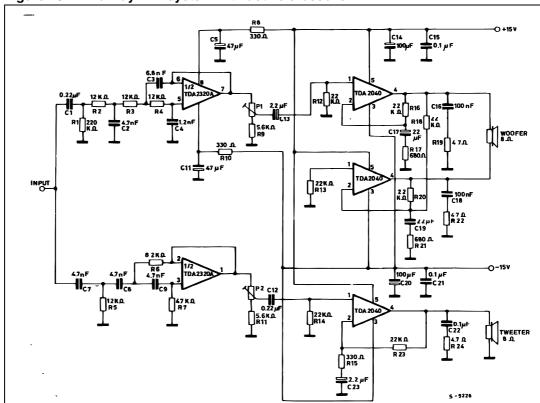
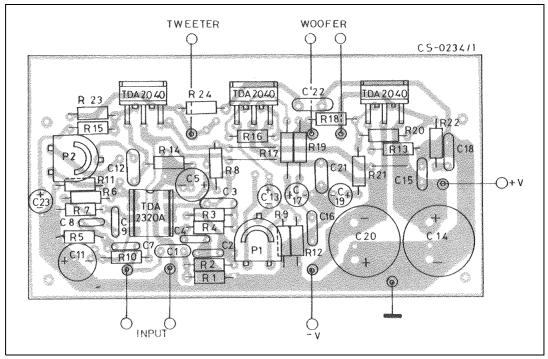


Figure 19. Two-way hi-fi system with active crossover

Figure 20. PCB and components layout for the circuit of the two-way hi-fi system with active crossover

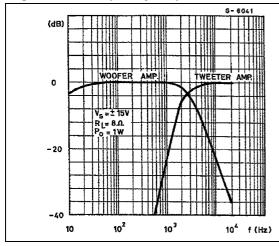


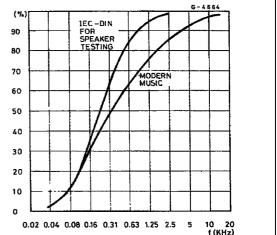
3.2 Multiway speaker systems and active boxes

Multiway loudspeaker systems provide the best possible acoustic performance since each loudspeaker is specially designed and optimized to handle a limited range of frequencies. Commonly, these loudspeaker systems divide the audio spectrum into two, three or four bands.

Figure 21. Frequency response

Figure 22. Power distribution vs. frequency





To maintain a flat frequency response over the hi-fi audio range the bands covered by each loudspeaker must overlap slightly. Any imbalance between the loudspeakers produces unacceptable results, therefore, it is important to ensure that each unit generates the correct amount of acoustic energy for its segment of the audio spectrum. In this respect it is also important to know the energy distribution of the music spectrum (see *Figure 22*) in order to determine the cutoff frequencies of the crossover filters. As an example, a 100-W three-way system with crossover frequencies of 400 Hz and 3 kHz would require 50 W for the woofer, 35 W for the midrange unit and 15 W for the tweeter.

Both active and passive filters can be used for crossovers but today active filters cost significantly less than a good passive filter using air-cored inductors and non-electrolytic capacitors. In addition, active filters do not suffer from the typical defects of passive filters:

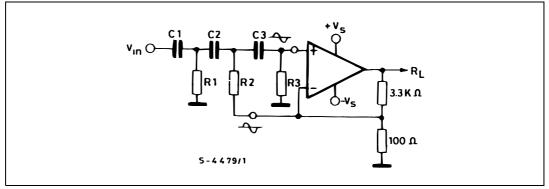
- power loss
- increased impedance seen by the loudspeaker (lower damping)
- difficulty of precise design due to variable loudspeaker impedance

Obviously, active crossovers can only be used if a power amplifier is provided for each drive unit. This makes it particularly interesting and economically sound to use monolithic power amplifiers.

In some applications, complex filters are not really necessary and simple RC low-pass and high-pass networks (6 dB/octave) can be recommended. The results obtained are excellent because this is the best type of audio filter and the only one free from phase and transient distortion. The rather poor out-of-band attenuation of single RC filters means that the loudspeaker must operate linearly well beyond the crossover frequency to avoid distortion.

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Figure 23. Active power filter



A more effective solution, named "Active Power Filter" by STMicroelectronics, is shown in *Figure 23*. The proposed circuit can be realized by combined power amplifiers and 12-dB/octave or 18-dB/octave high-pass or low-pass filters.

The component values calculated for fc = 900Hz using a Bessel 3rd order Sallen and Key structure are:

C1 = C2 = C3 = 22 nF

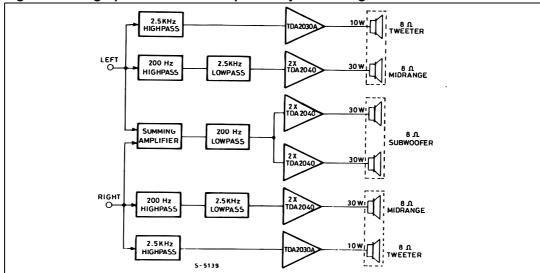
 $R1 = 8.2 \text{ k}\Omega$

 $R2 = 5.6 \text{ k}\Omega$

 $R3 = 33 \text{ k}\Omega$

In the block diagram of *Figure 24* is represented an active loudspeaker system completely realized using power integrated circuit, rather than the traditional discrete transistors on hybrids, very high quality is obtained by driving the audio spectrum into three bands using active crossovers (TDA2320A) and a separate amplifier and loudspeakers for each band. A modern subwoofer/midrange/tweeter solution is used.

Figure 24. High-power active loudspeaker system using TDA2030A and TDA2040



3.3 Pratical considerations

3.3.1 Printed circuit board

The layout shown in *Figure 14* should be adopted by the designers. If different layouts are used, the ground points of input 1 and input 2 must be well decoupled from the ground return of the output in which a high current flows.

3.3.2 Assembly suggestion

No electrical isolation is needed between the package and the heatsink with single supply voltage configuration.

3.3.3 Application suggestions

The recommended values of the components are those shown in the application circuit of *Figure 13*. However, if different values are chosen then the following table can be helpful.

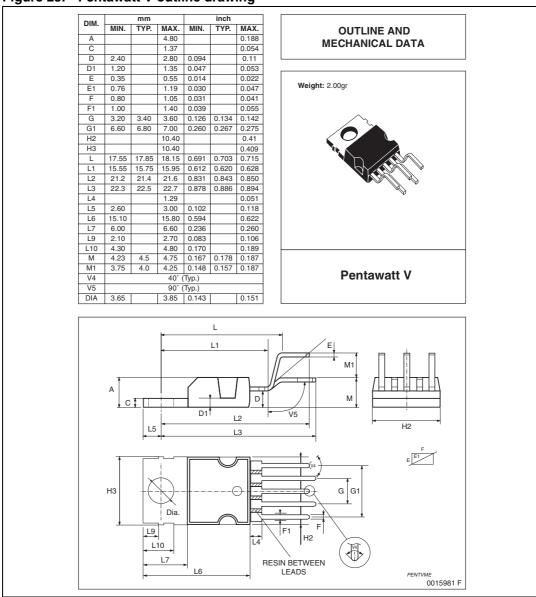
Table 5. Variations from recommended values

| Component | Recommended value | Purpose | Larger than recommended value | Smaller than recommended value |
|-----------|-------------------|-----------------------------|--|-----------------------------------|
| R1 | 22 kΩ | Non-inverting input biasing | Increase in input impedance | Decrease in input impedance |
| R2 | 680 Ω | Closed-loop gain setting | Decrease in gain ⁽¹⁾ | Increase in gain |
| R3 | 22 kΩ | Closed-loop gain setting | Increase in gain | Decrease in gain ⁽¹⁾ |
| R4 | 4.7 Ω | Frequency stability | Danger of oscillation at high frequencies with inductive loads | - |
| C1 | 1 μF | Input DC decoupling | - | Increase in low-frequency cut-off |
| C2 | 22 µF | Inverting DC decoupling | - | Increase in low-frequency cut-off |
| C3, C4 | 0.1 μF | Supply voltage bypass | - | Danger of oscillation |
| C5, C6 | 220μF | Supply voltage bypass | - | Danger of oscillation |
| C7 | 0.1μF | Frequency stability | - | Danger of oscillation |

^{1.} The value of closed loop gain must be higher than 24 ${\rm dB}$

4 Package mechanical data

Figure 25. Pentawatt V outline drawing



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TDA2040 Revision history

5 Revision history

Table 6. Document revision history

| Date | Revision | Changes | |
|-------------|----------|---|--|
| Apr-2003 | 3 | Changes not recorded | |
| 28-Oct-2010 | 4 | Added features list on page 1 Updated minimum supply voltage to ±4.5 V in <i>Table 4 on page 3</i> Corrected the title of <i>Figure 15 on page 8</i> Updated presentation | |
| 16-Jun-2011 | 5 | Removed minimum value from Pentawatt (vertical) package dimension H3 (<i>Figure 25</i>); minor textual changes. | |

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