



### 2.25 MHz 300 mA Step Down Converter in 2x2SON/TSOT23 Package

#### FEATURES

- High Efficiency Step Down Converter
- Output Current up to 300 mA
- V<sub>IN</sub> Range From 2 V to 6 V for Li-Ion Batteries With Extended Voltage Range
- 2.25 MHz Fixed Frequency Operation
- Power Save Mode at Light Load Currents
- Output Voltage Accuracy in PWM Mode ±1.5%
- Adjustable Output Voltage from 0.6 V to V<sub>IN</sub>
- Typical 15 μA Quiescent Current
- 100% Duty Cycle for Lowest Dropout
- Available in a TSOT23 and 2×2×0,8 mm SON

TPS62243DRV

SW

FB

VIN

ΕN

GND

MODE

 $L_1$ 

2.2µH

• Allows < 1 mm Solution Height

#### **APPLICATIONS**

- Bluetooth<sup>™</sup> Headset
- Cell Phones, Smart-phones
- WLAN
- PDAs, Pocket PCs
- Low Power DSP Supply
- Portable Media Players
- Digital Cameras

 $V_{IN} 2.0V$  to 6V

CIN

4.7µF



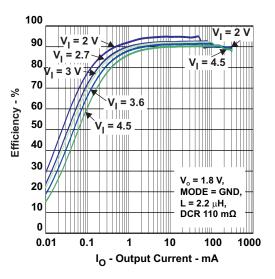
The TPS62240 device is a high efficiency synchronous step down dc-dc converter optimized for battery powered portable applications. It provides up to 300 mA output current from a single Li-Ion cell and is ideal to power portable applications like mobile phones and other portable equipment.

With an input voltage range of 2 V to 6 V, the device supports applications powered by Li-Ion batteries with extended voltage range, two- and three-cell alkaline, 3.3-V and 5-V input voltage rails.

The TPS62240 operates at 2.25 MHz fixed switching frequency and enters Power Save Mode operation at light load currents to maintain high efficiency over the entire load current range.

The Power Save Mode is optimized for low output voltage ripple. For low noise applications, the device can be forced into fixed frequency PWM mode by pulling the MODE pin high. In the shutdown mode, the current consumption is reduced to less than 1  $\mu A.$  TPS62240 allows the use of small inductors and capacitors to achieve a small solution size.

The TPS62240 is available in a 5-pin TSOT23 and 6-pin 2mm×2mm SON package.



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V<sub>OUT</sub> 1.8V

\_\_\_\_\_O V001 1.0V Up to 300mA

COUT

10µF

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PRODUCTION DATA information is current as of publication date. Products conform to specifications per the terms of the Texas Instruments standard warranty. Pro to or in the second date to the terms of the Texas in the terms of the terms of the texas necessarily include testing of all parameter.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### **ORDERING INFORMATION**

T <sub>A</sub>	PART NUMBER <sup>(1)</sup>	OUTPUT VOLTAGE <sup>(2)</sup>	PACKAGE <sup>(3)</sup>	PACKAGE DESIGNATOR	ORDERING	PACKAGE MARKING
	TPS62240	adjustable	TSOT23-5	DDC	TPS62240DDC	BYO
−40°C to	TPS62240	adjustable	SON 2x2 -6	DRV	TPS62240DRV	BYJ
85°C	TPS62242	1.2V fixed output voltage	SON 2x2 -6	DRV	TPS62242DRV	CCY
	TPS62243	1.8V fixed output voltage	SON 2x2 -6	DRV	TPS62243DRV	CBQ

The DDC (TSOT-23-5) and DRV (SON2x2) package are available in tape on reel. Add R suffix to order quantities of 3000 parts per reel.
 Contact TI for other fixed output voltage options.

(3) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

#### **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

			VALUE	UNIT
VI	Input voltage range <sup>(2)</sup>		–0.3 to 7	V
	Voltage range at EN, MODE		–0.3 to V <sub>IN</sub> +0.3, ≤7	V
	Voltage on SW		–0.3 to 7	V
	Peak output current		Internally limited	А
		HBM Human body model	2	kV
	ESD rating <sup>(3)</sup>	CDM Charge device model	1	ĸv
		Machine model	200	V
$T_{\rm J}$	Maximum operating junction temperature		-40 to 125	°C
T <sub>stg</sub>	Storage temperature range		-65 to 150	°C

(1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to network ground terminal.

(3) The human body model is a 100-pF capacitor discharged through a 1.5 kΩ resistor into each pin. The machine model is a 200-pF capacitor discharged directly into each pin.

#### **DISSIPATION RATINGS**

PACKAGE	R <sub>0JA</sub>	POWER RATING FOR T <sub>A</sub> ≤ 25°C	DERATING FACTOR ABOVE T <sub>A</sub> = 25°C
DDC	250°C/W	400 mW	4 mW/°C
DRV	76°C/W	1300 mW	13 mW/°C

#### **RECOMMENDED OPERATING CONDITIONS**

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
VI	Supply voltage, VIN	2		6	V
	Output voltage range for adjustable voltage	0.6		VIN	V
T <sub>A</sub>	Operating ambient temperature	-40		85	°C
TJ	Operating junction temperature	-40		125	°C

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#### **ELECTRICAL CHARACTERISTICS**

Over full operating ambient temperature range, typical values are at  $T_A = 25^{\circ}$ C. Unless otherwise noted, specifications apply for condition  $V_{IN} = EN = 3.6$ V. External components  $C_{IN} = 4,7\mu$ F 0603,  $C_{OUT} = 10\mu$ F 0603,  $L = 2.2\mu$ H, refer to parameter measurement information.

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
V <sub>IN</sub>	Input voltage range		2		6	V
	Output ourset	$2.3 \text{ V} \le \text{V}_{\text{IN}} \le 6 \text{ V}$			300	A
IOUT	Output current	$2 \vee \leq V_{IN} \leq 2.3 \vee$			150	mA
		I <sub>OUT</sub> = 0 mA. PFM mode enabled (MODE = GND) device not switching		15		A
l <sub>Q</sub> (	Operating quiescent current	$I_{OUT}$ = 0 mA. PFM mode enabled (MODE = GND) device switching, V <sub>OUT</sub> = 1.8 V, <sup>(1)</sup>		18.5		μA
		$I_{OUT}$ = 0 mA, switching with no load (MODE = V_{IN}), PWM operation , V_{OUT} = 1.8 V, V <sub>IN</sub> = 3 V		3.8		mA
I <sub>SD</sub>	Shutdown current	EN = GND		0.1	1	μA
UVLO	Lindon voltago lockout throshold	Falling		1.85		V
UVLU	Undervoltage lockout threshold	Rising		1.95		v
ENABLE,	MODE					
V <sub>IH</sub>	High level input voltage, EN, MODE	$2 V \le V_{IN} \le 6 V$	1		$V_{IN}$	V
V <sub>IL</sub>	Low level input voltage, EN, MODE	$2 V \le V_{IN} \le 6 V$	0		0.4	V
I <sub>IN</sub>	Input bias current, EN, MODE	EN, MODE = GND or VIN		0.01	1	μA
POWER S	WITCH					
D	High side MOSFET on-resistance			240	480	mΩ
R <sub>DS(on)</sub>	Low side MOSFET on-resistance	$-V_{IN} = V_{GS} = 3.6 \text{ V}, \text{ T}_{A} = 25^{\circ}\text{C}$		180	380	11122
I <sub>LIMF</sub>	Forward current limit MOSFET high-side and low side	VIN = VGS = 3.6 V	0.56	0.7	0.84	А
TSD	Thermal shutdown	Increasing junction temperature		140		°C
	Thermal shutdown hysteresis	Decreasing junction temperature		20		°C
OSCILLA	TOR					
f <sub>SW</sub>	Oscillator frequency	$2 V \le V_{IN} \le 6 V$	2	2.25	2.5	MHz
OUTPUT						
V <sub>OUT</sub>	Adjustable output voltage range		0.6		V <sub>IN</sub>	V
V <sub>ref</sub>	Reference Voltage			600		mV
	Feedback voltage	$\begin{array}{l} \mbox{MODE} = \mbox{V}_{IN}, \mbox{PWM operation}, \mbox{2 V} \leq \mbox{V}_{IN} \leq \mbox{6 V}, \mbox{in} \\ \mbox{fixed output voltage versions } \mbox{V}_{FB} = \mbox{V}_{OUT}, \mbox{ See }^{(2)} \end{array}$	-1.5%	0%	1.5%	
$V_{FB}$	Feedback voltage PFM mode	MODE = GND, device in PFM mode		0%		
	Load regulation			-0.5		%/A
t <sub>Start Up</sub>	Start-up Time	Time from active EN to reach 95% of V <sub>OUT</sub> nominal		500		μs
t <sub>Ramp</sub>	V <sub>OUT</sub> ramp UP time	Time to ramp from 5% to 95% of V <sub>OUT</sub>		250		μs
I <sub>lkg</sub>	Leakage current into SW pin	$V_{IN} = 3.6 \text{ V}, V_{IN} = V_{OUT} = V_{SW}, \text{ EN} = \text{GND},^{(3)}$		0.1	1	μA

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(1) See the parameter measurement information.

(2) for  $V_{IN} = V_O + 0.6$ 

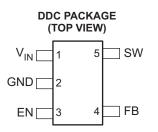
(3) In fixed output voltage versions, the internal resistor divider network is disconnected from FB pin.

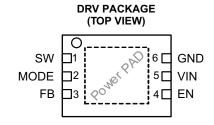
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#### PIN ASSIGNMENTS

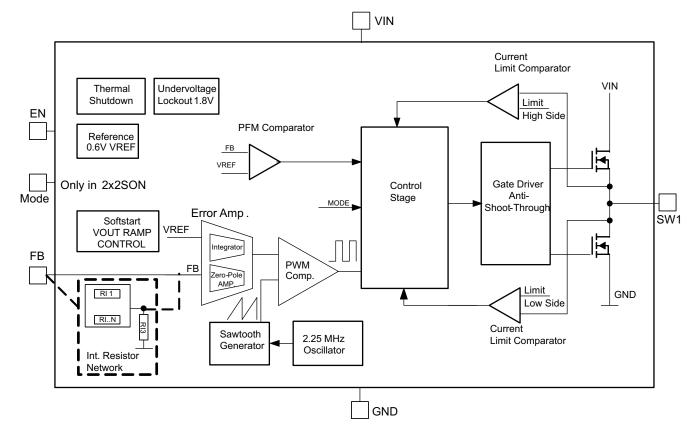




#### **TERMINAL FUNCTIONS**

	TERMIN	AL		
NAME	NO. (SON)	NO. TSTO23-5	I/O	DESCRIPTION
V <sub>IN</sub>	5	1	PWR	V <sub>IN</sub> power supply pin.
GND	6	2	PWR	GND supply pin
EN	4	3	I	This is the enable pin of the device. Pulling this pin to low forces the device into shutdown mode. Pulling this pin to high enables the device. This pin must be terminated.
SW	1	5	OUT	This is the switch pin and is connected to the internal MOSFET switches. Connect the inductor to this terminal.
FB	3	4	I	Feedback Pin for the internal regulation loop. Connect the external resistor divider to this pin. In case of fixed output voltage option, connect this pin directly to the output capacitor.
MODE	2		I	This pin is only available at SON package option. MODE pin = high forces the device to operate in fixed frequency PWM mode. MODE pin = low enables the Power Save Mode with automatic transition from PFM mode to fixed frequency PWM mode.

#### FUNCTIONAL BLOCK DIAGRAM

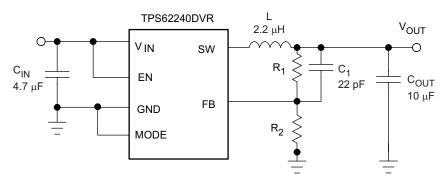


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#### PARAMETER MEASUREMENT INFORMATION



L: LPS3015 2.2  $\mu H,~110~m\Omega$   $C_{IN}$  GRM188R60J475K 4.7  $\mu F$  Murata 0603 size

 $C_{OUT}$  GRM188R60J106M 10  $\mu F$  Murata 0603 size

#### **TYPICAL CHARACTERISTICS**

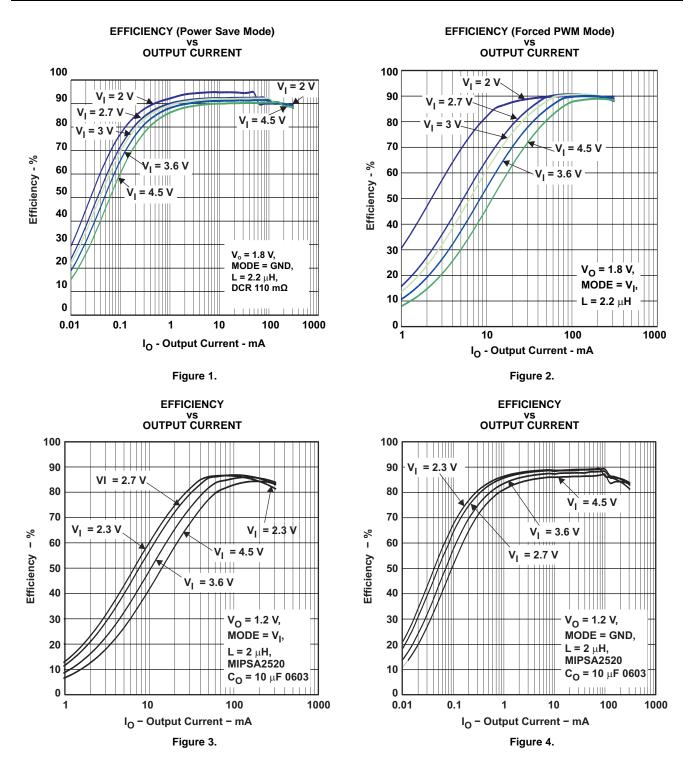
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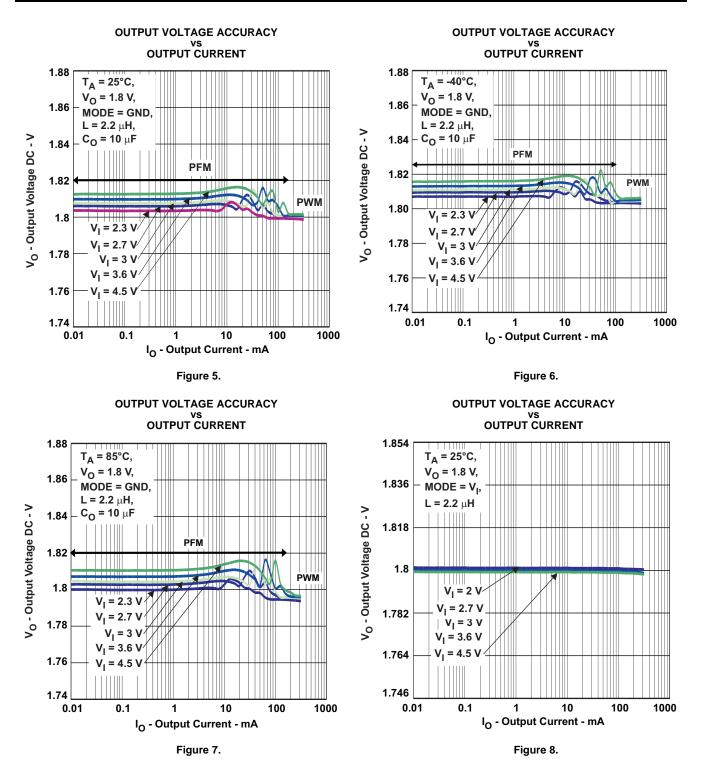
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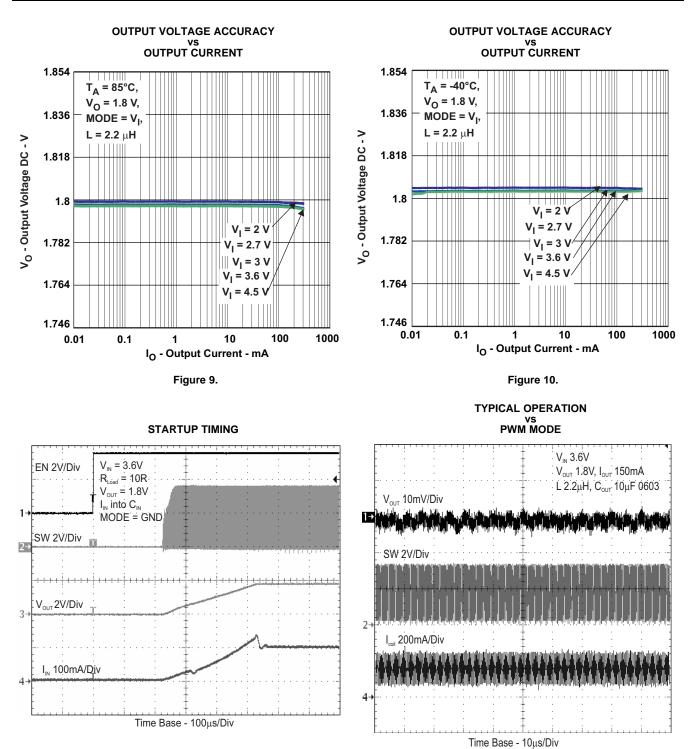
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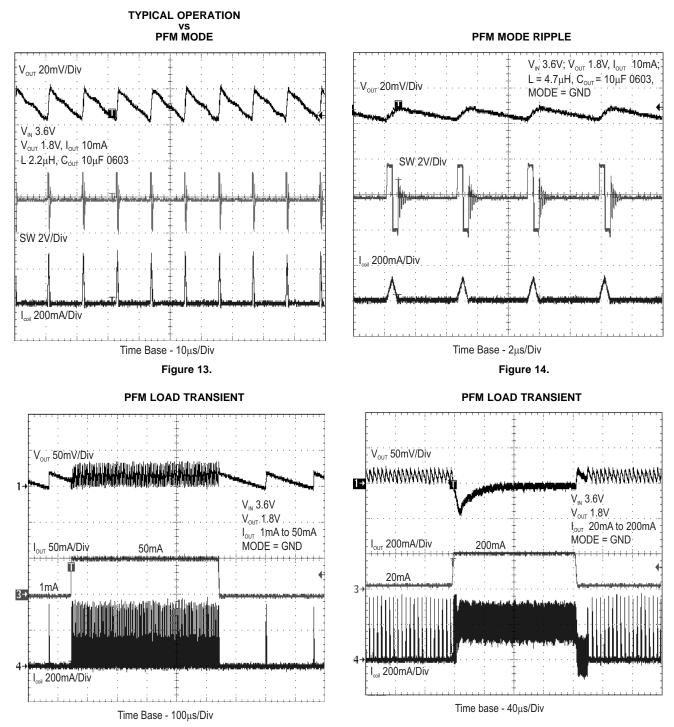


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Figure 12.



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Figure 16.

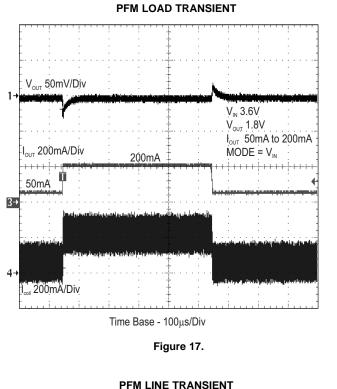
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#### PFM LINE TRANSIENT

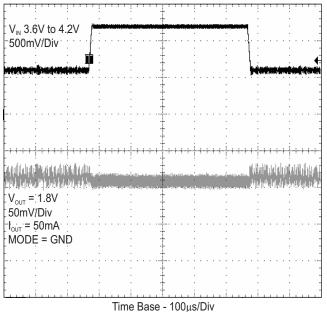
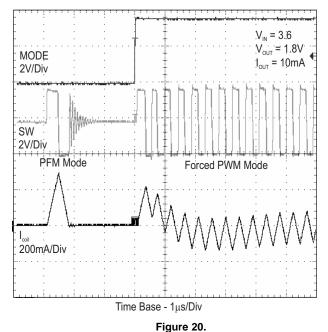
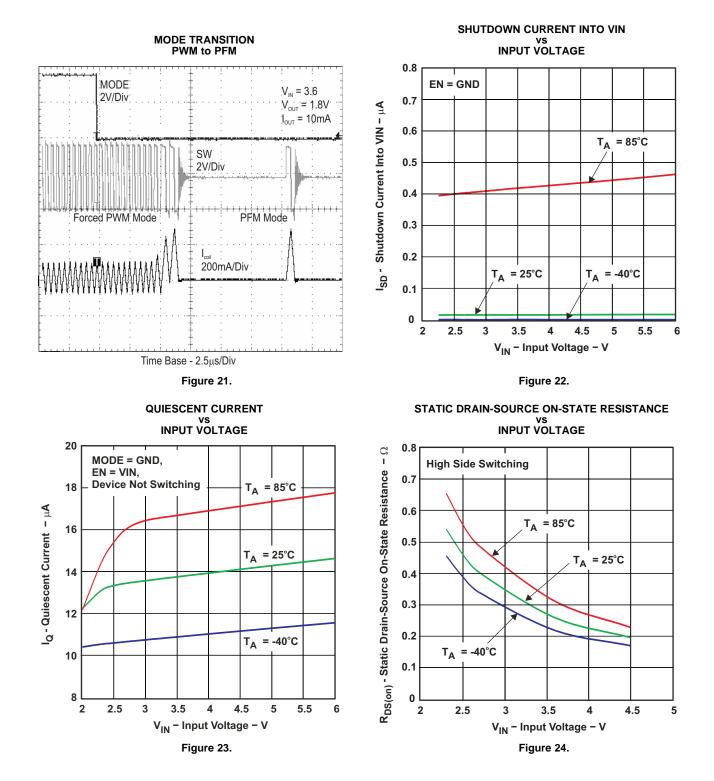


Figure 18.

#### MODE TRANSITION PFM to PWM



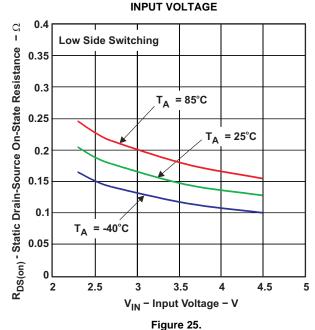


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#### STATIC DRAIN-SOURCE ON-STATE RESISTANCE vs INPUT VOLTAGE

#### DETAILED DESCRIPTION

#### OPERATION

The TPS62240 step down converter operates with typically 2.25MHz fixed frequency pulse width modulation (PWM) at moderate to heavy load currents. At light load currents, the converter can automatically enter Power Save Mode and operates then in PFM mode.

During PWM operation, the converter uses a unique fast response voltage mode control scheme with input voltage feed-forward to achieve good line and load regulation, allowing the use of small ceramic input and output capacitors. At the beginning of each clock cycle initiated by the clock signal, the High Side MOSFET switch is turned on. The current then flows from the input capacitor via the High Side MOSFET switch through the inductor to the output capacitor and load. During this phase, the current ramps up until the PWM comparator trips and the control logic turns off the switch. The current limit comparator also turns off the switch if the current limit of the High Side MOSFET switch is exceeded. After a dead time preventing shoot through current, the Low Side MOSFET rectifier is turned on and the inductor current ramps down. The current then flows from the inductor to the output capacitor and to the load. It returns back to the inductor through the Low Side MOSFET rectifier.

The next cycle is initiated by the clock signal again turning off the Low Side MOSFET rectifier and turning on the High Side MOSFET switch.

#### **POWER SAVE MODE**

The Power Save Mode is enabled with MODE Pin set to low level. If the load current decreases, the converter will enter Power Save Mode operation automatically. During Power Save Mode, the converter skips switching and operates with reduced frequency in PFM mode with a minimum quiescent current to maintain high efficiency.

The transition from PWM mode to PFM mode occurs once the inductor current in the Low Side MOSFET switch becomes zero, which indicates discontinuous conduction mode.

During the Power Save Mode, the output voltage is monitored with a PFM comparator. As the output voltage falls below the PFM comparator threshold of  $V_{OUT}$  nominal, the device starts a PFM current pulse. The High Side MOSFET switch will turn on, and the inductor current ramps up. After the On-time expires, the switch is turned off and the Low Side MOSFET switch is turned on until the inductor current becomes zero.

The converter effectively delivers a current to the output capacitor and the load. If the load is below the delivered current, the output voltage will rise. If the output voltage is equal to or greater than the PFM comparator threshold, the device stops switching and enters a sleep mode with typical 15-µA current consumption.

If the output voltage is still below the PFM comparator threshold, a sequence of further PFM current pulses are generated until the PFM comparator threshold is reached. The converter starts switching again once the output voltage drops below the PFM comparator threshold.

With a fast single-threshold comparator, the output voltage ripple during PFM mode operation can be kept to a minimum. The PFM Pulse is time controlled, allowing the user to modify the charge transferred to the output capacitor by the value of the inductor. The resulting PFM output voltage ripple and PFM frequency both depend on the size of the output capacitor and the inductor value. Increasing output capacitor values and inductor values will minimize the output ripple. The PFM frequency decreases with smaller inductor values and increases with larger values.

If the output current cannot be supported in PFM mode, the device exits PFM mode and enters PWM mode. The Power Save Mode can be disabled through the MODE pin set to high. The converter will then operate in fixed frequency PWM mode.

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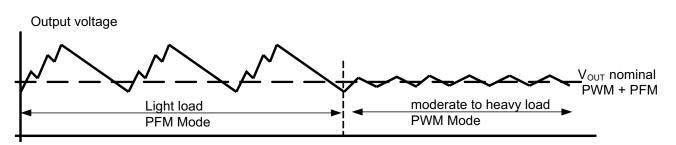


Figure 26. Power Save Mode

#### 100% Duty Cycle Low Dropout Operation

The device starts to enter 100% duty cycle mode once the input voltage comes close to the nominal output voltage. In order to maintain the output voltage, the High Side MOSFET switch is turned on 100% for one or more cycles.

With further decreasing  $V_{IN}$  the High Side MOSFET switch is turned on completely. In this case the converter offers a low input-to-output voltage difference. This is particularly useful in battery-powered applications to achieve longest operation time by taking full advantage of the entire battery voltage range.

The minimum input voltage to maintain regulation depends on the load current and output voltage, and can be calculated as:

 $V_{IN}min = V_{O}max + I_{O}max \times DSO(n)max + R_{L}$ 

With:

 $I_Omax = maximum output current plus inductor ripple current$  $<math>R_{DS(on)}max = maximum P$ -channel switch  $R_{DS(on)}$ .  $R_L = DC$  resistance of the inductor  $V_Omax = nominal output voltage plus maximum output voltage tolerance$ 

#### UNDERVOLTAGE LOCKOUT

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The undervoltage lockout circuit prevents the device from malfunctioning at low input voltages and from excessive discharge of the battery and disables the output stage of the converter. The undervoltage lockout threshold is typically 1.85V with falling  $V_{IN}$ .

#### MODE SELECTION

The MODE pin allows mode selection between forced PWM mode and Power Save Mode.

Connecting this pin to GND enables the Power Save Mode with an automatic transition between PWM and PFM mode. Pulling the MODE pin high forces the converter to operate in fixed frequency PWM mode even at light load currents. This allows simple filtering of the switching frequency for noise sensitive applications. In this mode, the efficiency is lower compared to the Power Save Mode during light loads.

The condition of the MODE pin can be changed during operation and allows efficient power management by adjusting the operation mode of the converter to the specific system requirements.

#### ENABLE

The device is enabled by setting the EN pin to high. During the start up time  $t_{Start Up}$ , the internal circuits are settled and the soft start circuit is activated. The EN input can be used to control power sequencing in a system with various dc/dc converters. The EN pin can be connected to the output of another converter, to drive the EN pin high and getting a sequencing of supply rails. With EN pin = GND, the device enters shutdown mode in which all circuits are disabled. In fixed output voltage versions, the internal resistor divider network is then disconnected from FB pin.

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#### SOFT START

The TPS62240 has an internal soft start circuit that controls the ramp up of the output voltage. The output voltage ramps up from 5% to 95% of its nominal value within typical  $250\mu$ s. This limits the inrush current in the converter during ramp up and prevents possible input voltage drops when a battery or high impedance power source is used. The soft start circuit is enabled within the start up time, t<sub>Start up</sub>.

#### SHORT-CIRCUIT PROTECTION

The High Side and Low Side MOSFET switches are short-circuit protected with maximum switch current equal to  $I_{LIMF}$ . The current in the switches is monitored by current limit comparators. Once the current in the High Side MOSFET switch exceeds the threshold of it's current limit comparator, it turns off and the Low Side MOSFET switch is activated to ramp down the current in the inductor and High Side MOSFET switch. The High Side MOSFET switch can only turn on again, once the current in the Low Side MOSFET switch has decreased below the threshold of its current limit comparator.

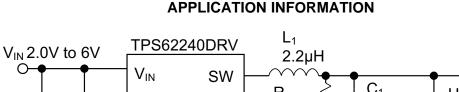
#### THERMAL SHUTDOWN

As soon as the junction temperature, T<sub>J</sub>, exceeds 140°C (typical) the device goes into thermal shutdown. In this mode, the High Side and Low Side MOSFETs are turned off. The device continues its operation when the junction temperature falls below the thermal shutdown hysteresis.

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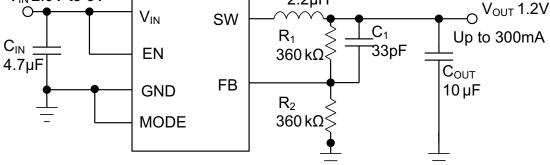
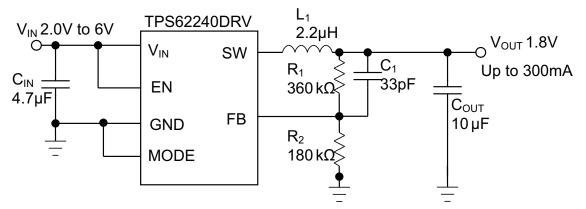


Figure 27. TPS62240DRV Adjustable 1.2 V





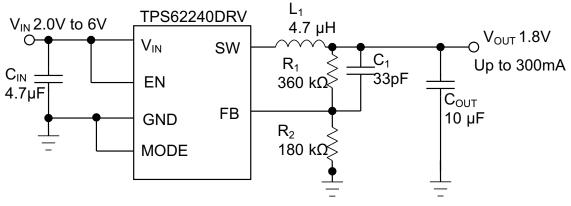


Figure 29. TPS62240DRV 1.8 V Low Ripple

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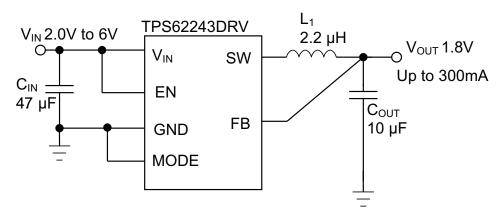


Figure 30. TPS62243 Fixed 1.8 V

#### **OUTPUT VOLTAGE SETTING**

The output voltage can be calculated to:

$$V_{OUT} = V_{REF} \times \left(1 + \frac{R_1}{R_2}\right)$$
 with an internal reference voltage  $V_{REF}$  typical 0.6 V

To minimize the current through the feedback divider network, R<sub>2</sub> should be 180 k $\Omega$  or 360 k $\Omega$ . The sum of R<sub>1</sub> and R<sub>2</sub> should not exceed ~1M $\Omega$ , to keep the network robust against noise.

An external feed forward capacitor  $C_1$  is required for optimum load transient response. The value of  $C_1$  should be in the range between 22pF and 33pF.

Route the FB line away from noise sources, such as the inductor or the SW line.

#### **OUTPUT FILTER DESIGN (INDUCTOR AND OUTPUT CAPACITOR)**

The TPS62240 is designed to operate with inductors in the range of  $1.5\mu$ H to  $4.7\mu$ H and with output capacitors in the range of  $4.7\mu$ F to  $22\mu$ F. The part is optimized for operation with a  $2.2\mu$ H inductor and  $10\mu$ F output capacitor.

Larger or smaller inductor values can be used to optimize the performance of the device for specific operation conditions. For stable operation, the L and C values of the output filter may not fall below  $1\mu$ H effective Inductance and  $3.5\mu$ F effective capacitance. Selecting larger capacitors is less critical because the corner frequency of the L-C filter moves to lower frequencies with fewer stability problems.

#### **Inductor Selection**

The inductor value has a direct effect on the ripple current. The selected inductor must be rated for its dc resistance and saturation current. The inductor ripple current ( $\Delta I_L$ ) decreases with higher inductance and increases with higher V<sub>1</sub> or V<sub>0</sub>.

The inductor selection also has an impact on the output voltage ripple in the PFM mode. Higher inductor values will lead to lower output voltage ripple and higher PFM frequency, and lower inductor values will lead to a higher output voltage ripple but lower PFM frequency.

Equation 1 calculates the maximum inductor current in PWM mode under static load conditions. The saturation current of the inductor should be rated higher than the maximum inductor current as calculated with Equation 2. This is recommended because during heavy load transients the inductor current will rise above the calculated value.

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$$\Delta I_{L} = Vout \times \frac{1 - \frac{Vout}{Vin}}{L \times f}$$
$$I_{Lmax} = I_{outmax} + \frac{\Delta I_{L}}{2}$$

With:

f = Switching Frequency (2.25 MHz typical)

L = Inductor Value

 $\Delta I_{I}$  = Peak to Peak inductor ripple current

I<sub>L max</sub> = Maximum Inductor current

A more conservative approach is to select the inductor current rating just for the maximum switch current limit I<sub>LIME</sub> of the converter.

Accepting larger values of ripple current allows the use of low inductance values, but results in higher output voltage ripple, greater core losses, and lower output current capability.

The total losses of the coil have a strong impact on the efficiency of the dc/dc conversion and consist of both the losses in the dc resistance (R<sub>(DC)</sub>) and the following frequency-dependent components:

- The losses in the core material (magnetic hysteresis loss, especially at high switching frequencies)
- Additional losses in the conductor from the skin effect (current displacement at high frequencies)
- Magnetic field losses of the neighboring windings (proximity effect)
- Radiation losses

DIMENSIONS [mm <sup>3</sup> ]	INDUCTANCE $\mu$ H	INDUCTOR TYPE	SUPPLIER
$2.5 \times 2.0 \times 1.0$	2.0	MIPS2520D2R2	FDK
$2.5 \times 2.0 \times 1.2$	2.0	MIPSA2520D2R2	FDK
2.5x2.0x1.0	2.2	KSLI-252010AG2R2	Hitachi Metals
2.5x2.0x1.2	2.2	LQM2HPN2R2MJ0L	Murata
$3 \times 3 \times 1.4$	2.2	LPS3015	Coilcraft

Table 1. List of Inductors

#### **Output Capacitor Selection**

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The advanced fast-response voltage mode control scheme of the TPS62240 allows the use of tiny ceramic capacitors. Ceramic capacitors with low ESR values have the lowest output voltage ripple and are recommended. The output capacitor requires either an X7R or X5R dielectric. Y5V and Z5U dielectric capacitors, aside from their wide variation in capacitance over temperature, become resistive at high frequencies.

At nominal load current, the device operates in PWM mode and the RMS ripple current is calculated as:

$$I_{\text{RMSCout}} = \text{Vout} \times \frac{1 - \frac{\text{Vout}}{\text{Vin}}}{L \times f} \times \frac{1}{2 \times \sqrt{3}}$$

At nominal load current, the device operates in PWM mode and the overall output voltage ripple is the sum of the voltage spike caused by the output capacitor ESR plus the voltage ripple caused by charging and discharging the output capacitor:

$$\Delta \text{Vout} = \text{Vout} \times \frac{1 - \frac{\text{Vout}}{\text{Vin}}}{\text{L} \times f} \times \left(\frac{1}{8 \times \text{Cout} \times f} + \text{ESR}\right)$$
(4)

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At light load currents, the converter operates in Power Save Mode and the output voltage ripple depends on the output capacitor and inductor value. Larger output capacitor and inductor values minimize the voltage ripple in PFM mode and tighten dc output accuracy in PFM mode.

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(1)

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#### **Input Capacitor Selection**

The buck converter has a natural pulsating input current; therefore, a low ESR input capacitor is required for best input voltage filtering, and minimizing the interference with other circuits caused by high input voltage spikes. For most applications, a 4.7- $\mu$ F to 10- $\mu$ F ceramic capacitor is recommended. Because ceramic capacitors lose up to 80% of their initial capacitance at 5V, it is recommended that a 10- $\mu$ F input capacitor be used for input voltages greater than 4.5V. The input capacitor can be increased without any limit for better input voltage filtering.

Take care when using only small ceramic input capacitors. When a ceramic capacitor is used at the input, and the power is being supplied through long wires, such as from a wall adapter, a load step at the output, or VIN step on the input, can induce ringing at the VIN pin. The ringing can couple to the output and be mistaken as loop instability, or could even damage the part by exceeding the maximum ratings

CAPACITANCE	TYPE	SIZE	SUPPLIER
4.7μF	GRM188R60J475K	0603: 1.6x0.8x0.8mm <sup>3</sup>	Murata
10μF	GRM188R60J106M69D	0603: 1.6x0.8x0.8mm <sup>3</sup>	Murata

#### Table 2. List of Capacitors

#### LAYOUT CONSIDERATIONS

As for all switching power supplies, the layout is an important step in the design. Proper function of the device demands careful attention to PCB layout. Care must be taken in board layout to get the specified performance. If the layout is not carefully done, the regulator could show poor line and/or load regulation, and additional stability issues as well as EMI problems. It is critical to provide a low inductance, impedance ground path. Therefore, use wide and short traces for the main current paths. The input capacitor should be placed as close as possible to the IC pins as well as the inductor and output capacitor.

Connect the GND pin of the device to the PowerPAD<sup>™</sup> land of the PCB and use this pad as a star point. Use a common Power GND node and a different node for the Signal GND to minimize the effects of ground noise. Connect these ground nodes together to the PowerPAD land (star point) underneath the IC. Keep the common path to the GND pin, which returns the small signal components, and the high current of the output capacitors as short as possible to avoid ground noise. The FB line should be connected right to the output capacitor and routed away from noisy components and traces (for example, the SW line).

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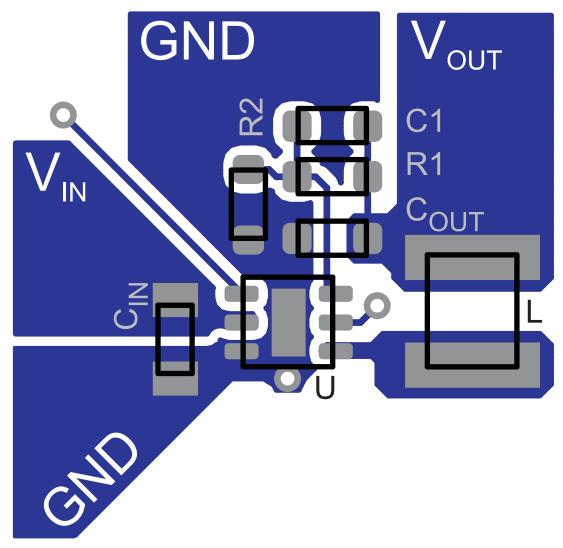


Figure 31. Layout

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26-Jan-2009

#### PACKAGING INFORMATION

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Packag Qty	e Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
TPS62240DDCR	ACTIVE	SOT	DDC	5	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DDCRG4	ACTIVE	SOT	DDC	5	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DDCT	ACTIVE	SOT	DDC	5	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DDCTG4	ACTIVE	SOT	DDC	5	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DRVR	ACTIVE	SON	DRV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DRVRG4	ACTIVE	SON	DRV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DRVT	ACTIVE	SON	DRV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62240DRVTG4	ACTIVE	SON	DRV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62242DRVR	ACTIVE	SON	DRV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62242DRVRG4	ACTIVE	SON	DRV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62242DRVT	ACTIVE	SON	DRV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62242DRVTG4	ACTIVE	SON	DRV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62243DRVR	ACTIVE	SON	DRV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62243DRVRG4	ACTIVE	SON	DRV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62243DRVT	ACTIVE	SON	DRV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TPS62243DRVTG4	ACTIVE	SON	DRV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

## Addendum-Page 1 www.BDTIC.com/TI

### PACKAGE OPTION ADDENDUM



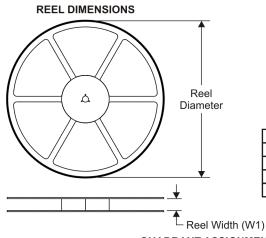
<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

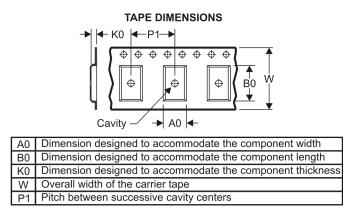
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#### TAPE AND REEL INFORMATION





#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

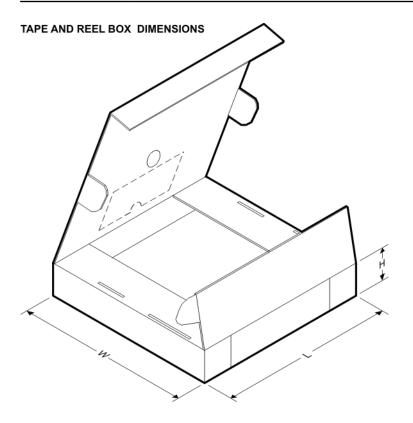


*All dimensions are nominal												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS62240DDCR	SOT	DDC	5	3000	179.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
TPS62240DDCT	SOT	DDC	5	250	179.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
TPS62240DRVR	SON	DRV	6	3000	179.0	8.4	2.2	2.2	1.2	4.0	8.0	Q2
TPS62240DRVT	SON	DRV	6	250	179.0	8.4	2.2	2.2	1.2	4.0	8.0	Q2
TPS62242DRVR	SON	DRV	6	3000	179.0	8.4	2.2	2.2	1.2	4.0	8.0	Q2
TPS62242DRVT	SON	DRV	6	250	179.0	8.4	2.2	2.2	1.2	4.0	8.0	Q2
TPS62243DRVR	SON	DRV	6	3000	179.0	8.4	2.2	2.2	1.2	4.0	8.0	Q2
TPS62243DRVT	SON	DRV	6	250	179.0	8.4	2.2	2.2	1.2	4.0	8.0	Q2



### PACKAGE MATERIALS INFORMATION

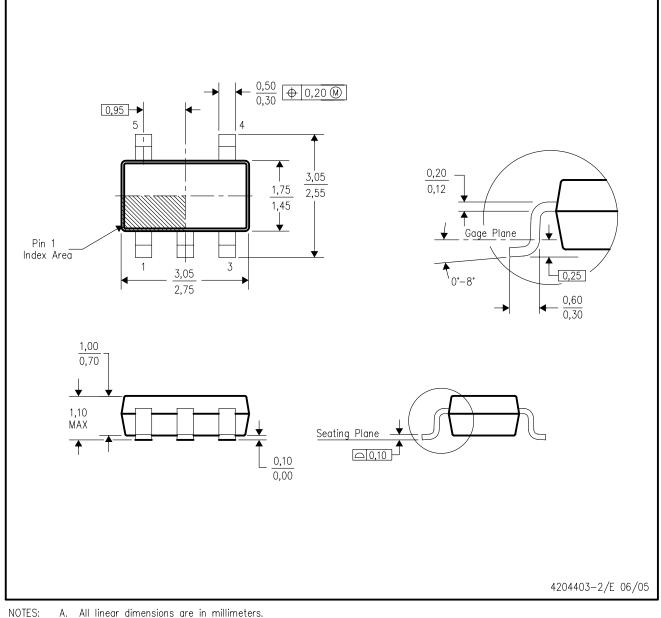
21-Feb-2009



Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS62240DDCR	SOT	DDC	5	3000	195.0	200.0	45.0
TPS62240DDCT	SOT	DDC	5	250	195.0	200.0	45.0
TPS62240DRVR	SON	DRV	6	3000	195.0	200.0	45.0
TPS62240DRVT	SON	DRV	6	250	195.0	200.0	45.0
TPS62242DRVR	SON	DRV	6	3000	195.0	200.0	45.0
TPS62242DRVT	SON	DRV	6	250	195.0	200.0	45.0
TPS62243DRVR	SON	DRV	6	3000	195.0	200.0	45.0
TPS62243DRVT	SON	DRV	6	250	195.0	200.0	45.0

DDC (R-PDSO-G5)

PLASTIC SMALL-OUTLINE

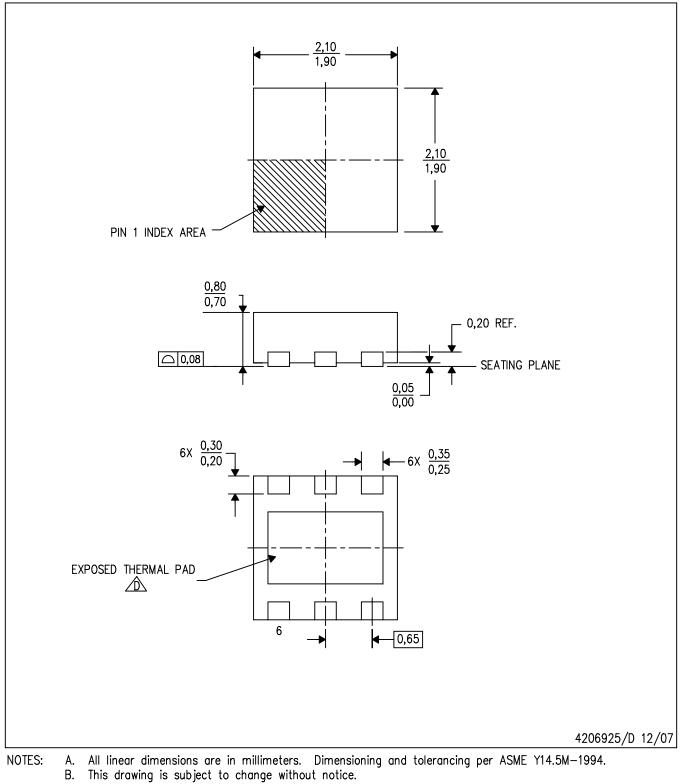


- - Β. This drawing is subject to change without notice.
  - C. Body dimensions do not include mold flash or protrusion.
  - D. Falls within JEDEC MO-193 variation AB (5 pin).



### **MECHANICAL DATA**





C. Small Outline No-Lead (SON) package configuration.

DRV (S-PDSO-N6)

The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.

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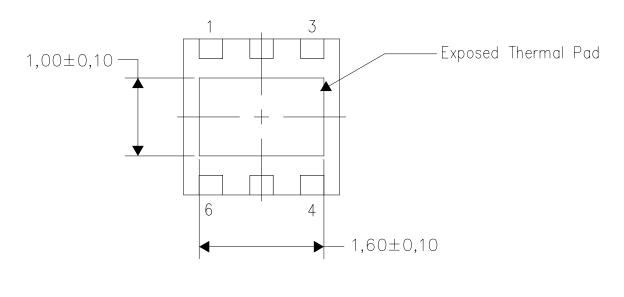


#### THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, Quad Flatpack No-Lead Logic Packages, Texas Instruments Literature No. SCBA017. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



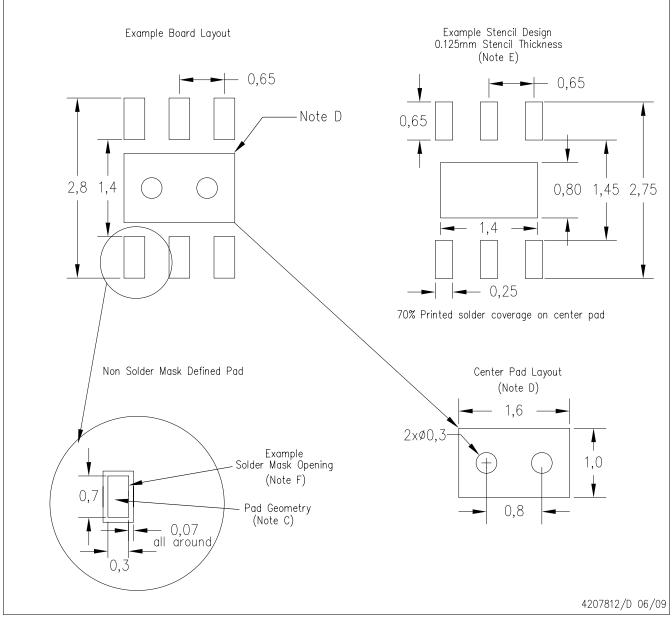
Bottom View

NOTE: All linear dimensions are in millimeters

Exposed Thermal Pad Dimensions

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## DRV (S-PWSON-N6)



NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Application Note, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC 7525 for stencil design considerations.
- F. Customers should contact their board fabrication site for solder mask tolerances.



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