

# DIGITALLY MANAGED PUSH-PULL ANALOG PWM CONTROLLERS

### **FEATURES**

- For Digitally Managed Power Supplies Using μCs or the TMS320 ™ DSP Family
- Voltage or Peak Current Mode Control with Cycle-by-Cycle Current Limiting
- Clock input from Digital Controller to set Operating Frequency and Max Duty Cycle
- Analog PWM Comparator
- 2-MHz Switching Frequency
- 110-V Input Startup Circuit and Thermal Shutdown (UCD8620)
- Internal Programmable Slope Compensation
- 3.3-V, 10-mA Linear Regulator
- DSP/μC Compatible Inputs
- Dual 4-A TrueDrive™ High Current Drivers
- 10-ns Typical Rise and Fall Times with 2.2-nF
- 25-ns Input-to-Output Propagation Delay
- 25-ns Current Sense-to-Output Propagation Delay
- Programmable Current Limit Threshold
- Digital Output Current Limit Flag
- 4.5-V to 15.5-V Supply Voltage Range
- Rated from -40C to 105C

### **APPLICATIONS**

- Digitally Managed Switch Mode Power Supplies
- Push-Pull, Half-Bridge, or Full-Bridge Converters
- Battery Chargers

# DESCRIPTION

The UCD8220 analog pulse-width modulator device is used in digitally managed power supplies using a microcontroller or the TMS320™ DSP family.

UCD8220 ia a double-ended PWM controller configured with push-pull drive logic.

Systems using the UCD8220 device close the PWM feedback loop with traditional analog methods, but the UCD8220 controller includes circuitry to interpret a time-domain digital pulse train. The pulse train contains the operating frequency and maximum duty cycle limit which are used to control the power supply operation. This eases implementation of a converter with high level control features without the added complexity or possible PWM resolution limitations of closing the control loop in the discrete time domain.

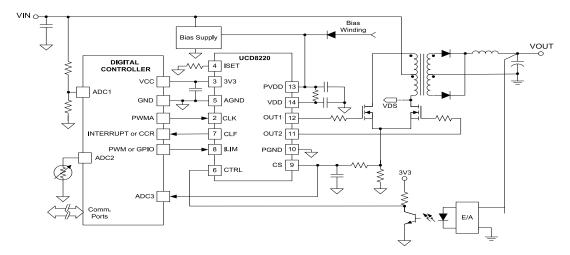


Figure 1. UCD8220 Typical Simplified Push-Pull Converter Application Schematic

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# **DESCRIPTION** (continued)

The UCD8220 can be configured for either peak current mode or voltage mode control. It provides a programmable current limit function and a digital output current limit flag which can be monitored by the host controller to set the current limit operation. For fast switching speeds, the output stage uses the TrueDrive™ architecture, which delivers rated current of 4 A into the gate of a MOSFET. Finally it also includes a 3.3-V, 10-mA linear regulator to provide power to the digital controller or act as a reference in the system.

The UCD8220 controller is compatible with the standard 3.3-V I/O ports of UCD9K digital power controllers, DSPs, Microcontrollers, or ASICs and is offered in PowerPAD™ HTSSOP and QFN packages.

# SIMPLIFIED APPLICATION DIAGRAMS

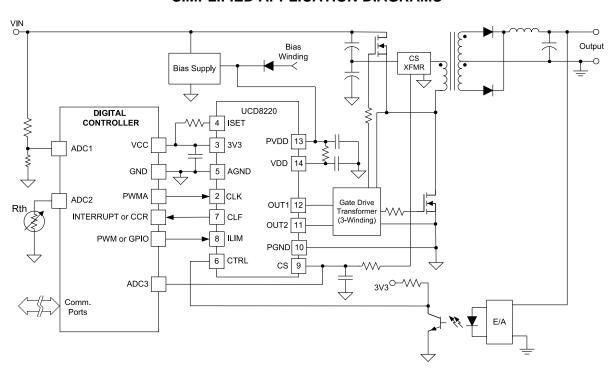


Figure 2. UCD8220 Typical Simplified Half-Bridge Converter Application Schematic

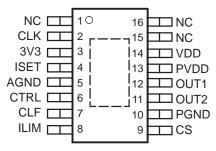




These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

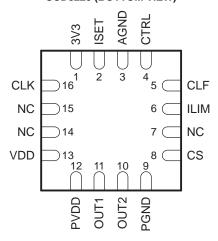
# **CONNECTION DIAGRAMS**

### HTSSOP PACKAGE (PWP -16) UCD8220 (TOP VIEW)



NC - No internal connection

### QFN PACKAGE (RSA-16) UCD8220 (BOTTOM VIEW)



### ORDERING INFORMATION

	110-V HV STARTUP	PACKAGED DEVICES(1)(2)(3)						
TEMPERATURE RANGE	CIRCUIT	PowerPAD™ HTSSOP-16 (PWP)	QFN-16 (RSA) <sup>(4)</sup>	QFN-20 (RGW)				
-40C to 105C	No	UCD8220PWP	UCD8220RSA	-				

- (1) HTSSOP-16 (PWP), QFN-16 (RSA), and QFN-20 (RGW) packages are available taped and reeled. Add R suffix to device type (e.g. UCD8220PWPR) to order quantities of 2,000 devices per reel for the PWP package and 1,000 devices per reel for the RSA and RGW packages.
- (2) These products are packaged in Pb-Free and Green lead finish of Pd-Ni-Au which is compatible with MSL level 1 at 255C to 260C peak reflow temperature to be compatible with either lead free or Sn/Pb soldering operations.
- (3) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI Web site at www.ti.com.
- (4) Contact factory for availability of QFN packaging.



### **PACKAGING INFORMATION**

PACKAGE	SUFFIX	θ <sub>JC</sub> (°C/W)	θ <sub>JA</sub> (°C/W)	POWER RATING T <sub>A</sub> = 70°C, T <sub>J</sub> = 125°C (mW)	RATING FACTOR ABOVE 70°C (mW/°C)
PowerPad™ MSSOP-16	PWP	2.07	37.47 <sup>(1)</sup>	1470	27
QFN-16	RSA	-	-	-	-
QFN-20	RGW	-	-	-	-

PowerPad<sup>™</sup> soldered to the PWB with TI recommended PWB as defined in TI's Application Report (TI Literature Number SLMA002) with OLFM.

# **ABSOLUTE MAXIMUM RATINGS**(1)(2)

SYMBOL		PARAMETER	UCD8x20	UNIT	
$V_{DD}$	Supply Voltage		16	V	
1	Cumply Current	Quiescent	20	A	
I <sub>DD</sub>	Supply Current	Switching, $T_A = 25^{\circ}C$ , $T_J = 125^{\circ}C$ , $V_{DD} = 12 \text{ V}$	200	- mA	
Vo	Output Gate Drive Voltage	OUT	-1 to PVDD	V	
I <sub>O(sink)</sub>	Output Cata Drive Current	OUT	4.0	- A	
I <sub>O(source)</sub>	Output Gate Drive Current	001	-4.0		
	Analog Input	ISET, CS, CTRL, ILIM	-0.3 to 3.6	V	
	Digital I/O's	CLK, CLF	-0.3 to 3.6		
		$T_A = 25C \text{ (PWP-16 package)}$		10/	
	Power Dissipation	ower Dissipation T <sub>A</sub> = 25C (QFN-16 package)		W	
		T <sub>A</sub> = 25C (QFN-20 package)	-		
T <sub>J</sub>	Junction Operating Temperature	' '		С	
T <sub>stg</sub>	Storage Temperature		-65 to 150		
HBM	ESD Rating <sup>(3)</sup>	Human body model	2000		
CDM	ESD Rating (-)	Charged device model	500	V	
	Lead Temperature (Soldering	300	С		

<sup>(1)</sup> Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

<sup>(2)</sup> All voltages are with respect to GND. Currents are positive into, negative out of the specified terminal.

<sup>(3)</sup> Tested to JEDEC standard EIA/JESD22 - A114-B.



# **ELECTRICAL CHARACTERISTICS**

 $V_{DD}$  = 12 V, 4.7-F capacitor from  $V_{DD}$  to AGND, 1  $\mu$ F from PVDD to PGND, 0.22-F capacitor from 3V3 to AGND,  $T_A = T_J = -40$ C to 105C, (unless otherwise noted).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY SECTION					
Supply current, OFF	V <sub>DD</sub> = 4.2 V		300	500	Α
Supply current, ON	(UCD8220), outputs not switching, CLK = low	2		3	mA
LOW VOLTAGE UNDERVOLTAGE L	OCKOUT (UCD8220 only)				
V <sub>DD</sub> UVLO ON		4.25	4.5	4.75	V
V <sub>DD</sub> UVLO OFF		4.05	4.25	4.45	V
V <sub>DD</sub> UVLO hysteresis		150	250	350	mV
REFERENCE / EXTERNAL BIAS SU	PPLY				
3V3 initial set point	$T_A = 25C, I_{LOAD} = 0$	3.267	3.3	3.333	V
3V3 set point over temperature		3.234	3.3	3.366	V
3V3 load regulation	I <sub>LOAD</sub> = 1 mA to 10 mA, VDD = 5 V	=	1	6.6	mV
3V3 line regulation	VDD = 4.75 V to 12 V, I <sub>LOAD</sub> = 10 mA	=	1	6.6	IIIV
Short circuit current	VDD = 4.75 to 12 V	11	20	35	mA
3V3 OK threshold, ON	3.3 V rising	2.9	3.0	3.1	V
3V3 OK threshold, OFF	3.3 V falling	2.7	2.8	2.9	V
CLOCK INPUT (CLK)					
HIGH, positive-going input threshold voltage (VIT+)		1.65	-	2.08	
LOW negative-going input threshold voltage (VIT-)		1.16	-	1.5	V
Input voltage hysteresis, (VIT+ - VIT-)		0.6	-	0.8	
Frequency	OUTx = 1 MHz	-	-	2	MHz
Minimum allowable off time (1)				20	ns
SLOPE COMPENSATION (ISET)					
ISET Voltage	V <sub>ISET</sub> , 3V3 = 3.3 V, +/-2%	1.78	1.84	1.90	V
	$R_{ISET}$ = 6.19 k $\Omega$ to AGND, CS = 0.25 V, CTRL = 2.5 V	1.48	2.12	2.76	
m, V <sub>SLOPE</sub> (I-Mode)	$R_{ISET}$ = 100 k $\Omega$ to AGND, CS = 0.25 V, CTRL = 2.5 V	0.099	0.142	0.185	
	$R_{ISET}$ = 499 k $\Omega$ to AGND, CS = 0.25 V, CTRL = 2.5 V	0.019	0.028	0.037	1//-
	$R_{ISET}$ = 4.99 k $\Omega$ to 3V3, CTRL = 2.5 V	1.44	2.06	2.68	V/s
m, V <sub>SLOPE</sub> (V-Mode)	$R_{ISET}$ = 100 k $\Omega$ to 3V3, CTRL = 2.5 V	0.079	0.114	0.148	
	$R_{ISET}$ = 402 k $\Omega$ to 3v3, CTRL = 2.5 V	0.019	0.027	0.035	
ISET resistor range	Current mode control; R <sub>ISET</sub> connected to AGND	6.19		499	1.0
ISET resistor range	Voltage mode control; R <sub>ISET</sub> connected to 3V3	4.99		402	kΩ
ISET current range	Voltage mode control with Feed-Forward; R <sub>ISET</sub> connected to VIN	3.7		300	μΑ
PWM					
PWM offset at CTRL input	3V3 = 3.3 V +/-2%	0.45	0.51	0.6	V
CTRL buffer gain <sup>(1)</sup>	Gain from CTRL to PWM comparator input		0.5		V/V
CURRENT LIMIT (ILIM)				l.	
ILIM internal current limit threshold	ILIM = OPEN	0.466	0.5	0.536	V
ILIM maximum current limit threshold	ILIM = 3.3 V	0.975	1.025	1.075	17
ILIM current limit threshold	ILIM = 0.75 V	0.700	0.725	0.750	V
ILIM minimum current limit threshold	ILIM = 0.25 V	0.21	0.23	0.25	V

<sup>(1)</sup> Ensured by design. Not 100% tested in production.



 $V_{DD}$  = 12 V, 4.7-F capacitor from  $V_{DD}$  to AGND, 1  $\mu$ F from PVDD to PGND, 0.22-F capacitor from 3V3 to AGND,  $T_A = T_J = -40C$  to 105C, (unless otherwise noted).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
CLF output high level	CS > ILIM , I <sub>LOAD</sub> = -7 mA	2.64	-	-	V
CLF output low level	CS ≤ ILIM, I <sub>LOAD</sub> = 7 mA	=	-	0.66	V
Propagation delay from CLK to CLF	CLK rising to CLF falling after a current limit event	=	15	25	ns
CURRENT SENSE COMPARATOR					
Bias voltage	Includes CS comp offset	5	25	50	mV
Input bias current		=	-1	-	μΑ
Propagation delay from CS to OUTx	ILIM = 0.5 V, measured on OUTx, CS = threshold + 60 mV	=	25	40	20
Propagation delay from CS to CLF	ILIM = 0.5 V, measured on CLF, CS = threshold + 60 mV	=	25	50	ns
CURRENT SENSE DISCHARGE TRA					
Discharge resistance	CLK = low, resistance from CS to AGND	10	35	75	Ω
OUTPUT DRIVERS					
Source current (2)	V <sub>DD</sub> = 12 V, CLK = high, OUTx = 5 V	=	4	-	
Sink current (2)	V <sub>DD</sub> = 12 V, CLK = low, OUTx = 5 V	-	4	-	^
Source current <sup>(2)</sup>	$V_{DD} = 4.75 \text{ V}, \text{ CLK} = \text{high, OUTx} = 0$	-	2	-	Α
Sink current (2)	V <sub>DD</sub> = 4.75 V, CLK = low, OUTx = 4.75 V	-	3	-	
Rise time, t <sub>R</sub>	C <sub>LOAD</sub> = 2.2 nF, V <sub>DD</sub> = 12 V	-	10	20	
Fall time, t <sub>F</sub>	$C_{LOAD} = 2.2 \text{ nF}, V_{DD} = 12 \text{ V}$	=	10	15	ns
Output with V <sub>DD</sub> < UVLO	V <sub>DD</sub> = 1.0 V, I <sub>SINK</sub> = 10 mA	=	0.8	1.2	V
Proposition doloy from CLK to OLITY	C <sub>LOAD</sub> = open, V <sub>DD</sub> = 12 V, CLK rising, t <sub>D1</sub>	-	25	35	20
Propagation delay from CLK to OUTx	C <sub>LOAD</sub> = open, V <sub>DD</sub> = 12 V, CLK falling, t <sub>D2</sub>		25	35	ns

(2) Ensured by design. Not 100% tested in production.

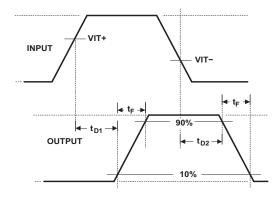


Figure 3. Timing Diagram



# **FUNCTIONAL BLOCK DIAGRAMS**

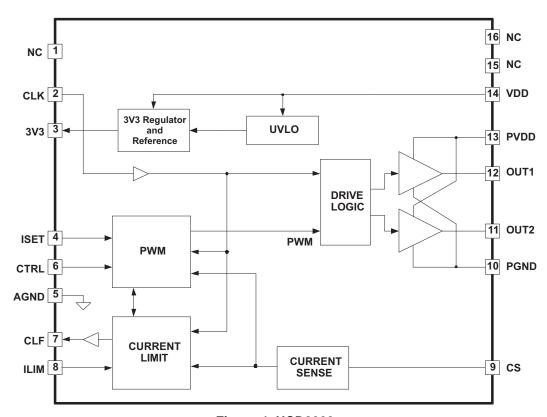


Figure 4. UCD8220

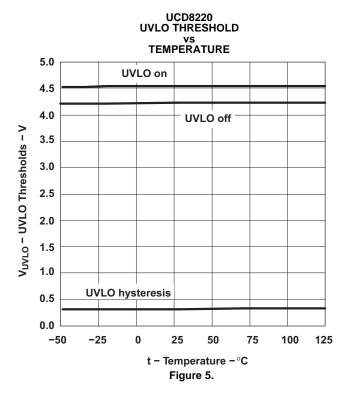
# **TERMINAL FUNCTIONS**

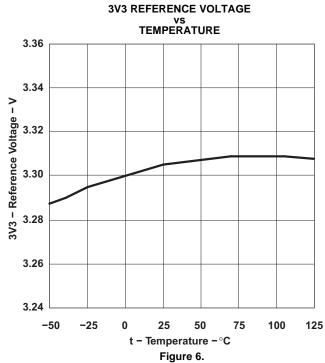
	PIN NUM	IBER						
PIN NAME	UCD82	UCD8220		UCD8220		UCD8220		FUNCTION
FIN NAME	HTSSOP-16 (PWP)	QFN-16 (RSA)	1/0	FUNCTION				
CLK	2	16	ı	Clock. Input pulse train contains operating frequency and maximum duty cycle limit. This pin is a high impedance digital input capable of accepting 3.3-V logic level signals up to 2 MHz. There is an internal Schmitt trigger comparator which isolates the internal circuitry from any external noise.				
CLF	7	5	0	Current limit flag. When the CS level is greater than the ILIM voltage minus 25 mV, the output driver is forced low and the current limit flag (CLF) is set high. The CLF signal is latched high until the device receives the next rising edge on the CLK pin. This signal is also used for the start-up handshaking between the Digital controller and the analog controller				
ISET	4	2	I	Pin for programming the current used to set the amount of slope compensation in Peak-Current Mode control or to set the internal capacitor charging in voltage mode control.				
3V3	3	1	0	Regulated 3.3-V rail. The onboard linear voltage regulator is capable of sourcing up to 10 mA of current. Place $0.22~\mu\text{F}$ of ceramic capacitance from this pin to analog ground.				
AGND	5	3	-	Analog ground return				
ILIM	8	6	I	Current limit threshold set pin. The current limit threshold can be set to any value between 0.25 V and 1.0 V. The default value while open is 0.5 V.				
CTRL	6	4	I	Input for the error feedback voltage from the external error amplifier. This input is multiplied by 0.5 and routed to the negative input of the PWM comparator				
NC	1, 15, 16	7, 14, 15	-	No connection.				
CS	9	8	I	Current sense pin. Fast current limit comparator connected to the CS pin is used to protect the power stage by implementing cycle-by-cycle current limiting.				
PGND	10	9	-	Power ground return. This pin should be connected close to the source of the power MOSFET.				
OUT2	11	10	0	The high-current TrueDrive™ driver output.				
OUT1	12	11	0	The high-current TrueDrive™ driver output.				



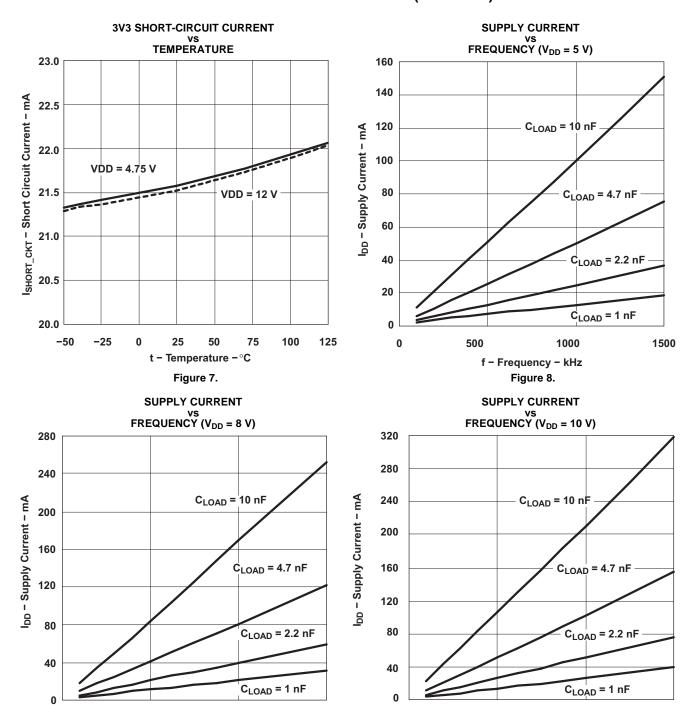
	PIN NUM	BER		
PIN NAME	UCD8220		1/0	FUNCTION
	HTSSOP-16 (PWP)	QFN-16 (RSA)	,,,	
PVDD	13	12		Supply pin provides power for the output drivers. It is not connected internally to the VDD supply rail. The bypass capacitor for this pin should be returned to PGND.
VDD	14	13	I	Supply input pin to power the control circuitry. Bypass the pin with at least 4.7 $\mu\text{F}$ of capacitance, returned to AGND.
VIN	-	=	I	Input to the internal start-up circuitry rated to 110 V. This pin connects directly to the input power rail.

# **TYPICAL CHARACTERISTICS**









1500

500

1000

f - Frequency - kHz Figure 9.

0

0

500

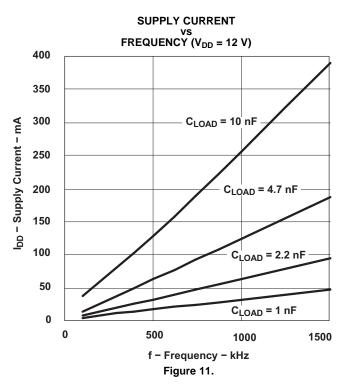
f - Frequency - kHz

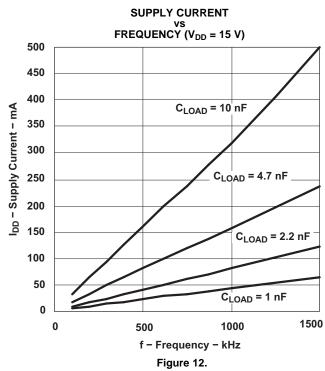
Figure 10.

1500

1000

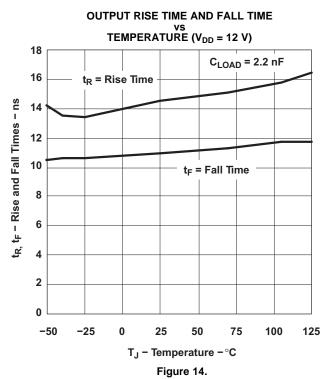




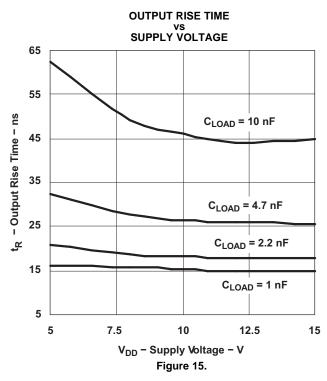


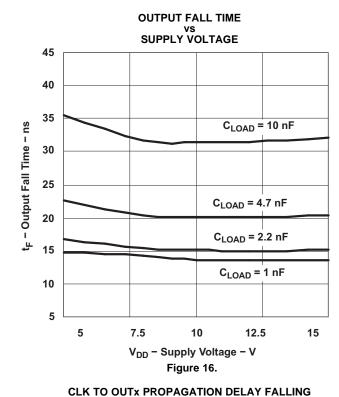
# **CLK INPUT THRESHOLD** vs TEMPERATURE 2.5 **CLK Input Rising** 2.0 V<sub>1</sub> – CLK Input Voltage – V 1.5 **CLK Input Falling** 1.0 0.5 0.0 0 50 100 -50 -25 25 75 125 T<sub>J</sub> - Temperature -°C

Figure 13.

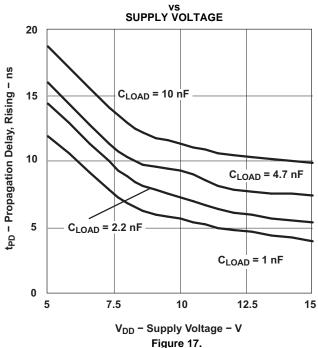








# **CLK to OUTx PROPAGATION DELAY RISING**



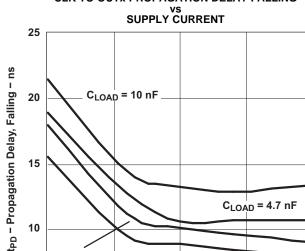
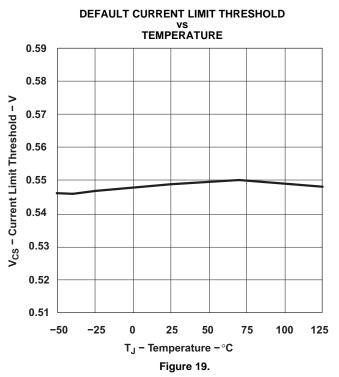
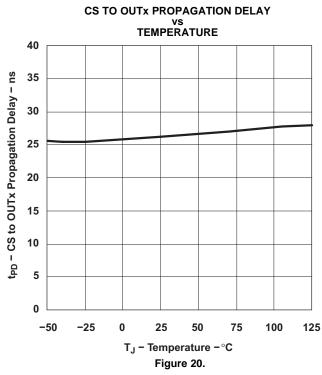
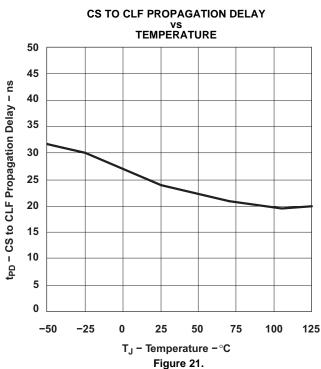


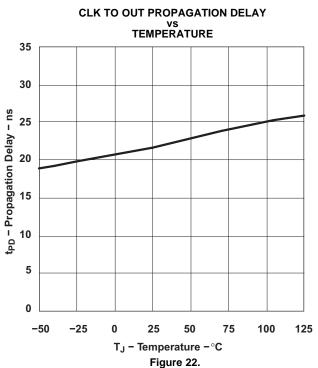
Figure 18.



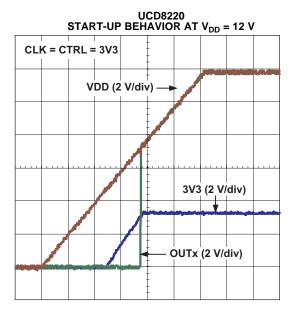




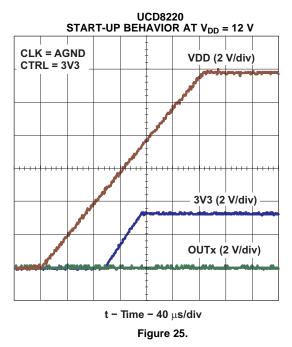


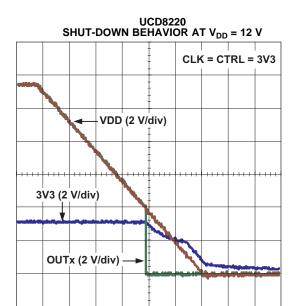




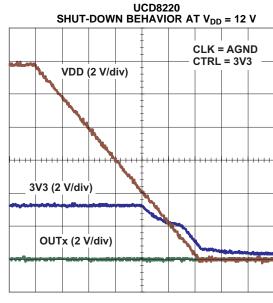


t – Time – 40  $\mu$ s/div Figure 23.



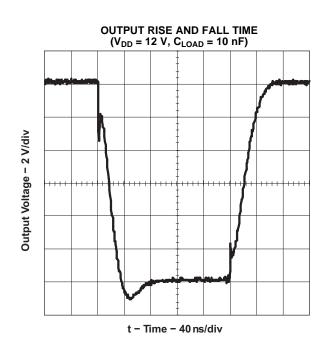


t - Time - 40  $\mu$ s/div Figure 24.



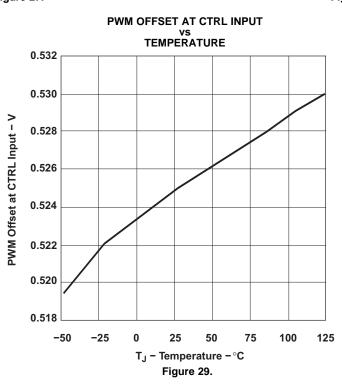
t - Time - 40  $\mu$ s/div Figure 26.





# INTERNAL SLOPE COMPENSATION IN CMC vs TEMPERATURE 0.146 **Current Mode Slope,** R<sub>ISET</sub> = 100 k Internal Slope Compensation in CMC - V/µs 0.144 0.142 0.140 0.138 0.136 0.134 -50 -25 25 50 75 100 125 T<sub>J</sub> - Temperature - °C Figure 28.

Figure 27.





### **APPLICATION INFORMATION**

#### Introduction

The UCD8220 is a digitally managed analog PWM controller configured with push-pull drive logic.

In systems using the UCD8220 device, the PWM feedback loop is closed using the traditional analog methods, but the UCD8220 includes circuitry to interpret a time-domain digital pulse train from a digital controller. The pulse train contains the operating frequency and maximum duty cycle limit and hence controls the power supply operation. This eases implementing a converter with high-level control features without the added complexity or digital PWM resolution limitations encountered when closing the voltage control loop in the discrete time domain.

The UCD8220 can be configured for either peak current mode or voltage mode control. It provides a programmable current limit function and a digital output current limit flag which can be monitored by the host controller. For fast switching speeds, the output stages use the TrueDrive™ output architecture, which delivers rated current of 4 A into the gate of a MOSFET during the Miller plateau region of the switching transition. Finally they also include a 3.3-V, 10-mA linear regulator to provide power for the digital controller.

The UCD8220 includes circuitry and features to ease implementing a converter that is managed by a microcontroller or a digital signal processor. Digitally managed power supplies provide software programmability and monitoring capability of a power supply's operation including:

- Switching frequency
- Synchronization
- D<sub>MAX</sub>
- V x S clamp
- Input UVLO start/stop voltage
- Input OVP start/stop voltage
- Soft-start profile
- Current limit operation
- Shutdown
- Temperature shutdown

# CLK Input Time-Domain Digital Pulse Train

While the loop is closed in the analog domain, the UCD8220 is managed by a time-domain digital pulse train from a digital controller. The pulse train, shown as CLK in Figure 30, contains the operating frequency and maximum duty cycle limit and hence controls the power supply operation as listed above.

The pulse train uses a Texas Instruments communication protocol which is a proprietary communication system that provides handles for control of the power supply operation through software programming. The rising edge of the CLK signal represents the switching frequency. Figure 30 depicts the operation of the UCD8220 in one of 5 modes. At the time when the internal signal REF OK is low, the UCD8220 is not ready to accept CLK inputs. Once the REF OK signal goes high, then the device is ready to process inputs. While the CLK input is low, the outputs are disabled and the CLK signal is used as an enable input. Once the Digital controller completes its initialization routine and verifies that all voltages are within their operating range, then it starts the soft-start procedure by slowly ramping up the duty cycle of the CLK signal, while maintaining the desired switching frequency. The CLK duty cycle continues to increase until it reaches steady-state where the analog control loop takes over and regulates the output voltage to the desired set point. During steady state, the duty cycle of the CLK pulse can be set using a volt second product calculation in order to protect the primary of the power transformer from saturation during transients.

When the power supply enters current limit, the outputs are quickly turned off, and the CLF signal is set high in order to notify the digital controller that the last power pulse was truncated because of an overcurrent event. The benefit of this technique is in the flexibility it offers.

The software is now in charge of the response to overcurrent events. In typical analog designs, the power supply response to overcurrent is hardwired in the silicon. With this method, the user can configure the response differently for different applications. For example, the software can be configured to latch-off the power supply in response the first overcurrent event, or to allow a fixed number of current limit events, so that the supply is capable of starting up into a capacitive load. The user can also configure the supply to enter into hiccup mode immediately or after a certain number of current limit events. As described later in this data sheet, the current limit threshold can be varied in time to create unique current limit profiles. For example, the current limit set point can be set high for a predefined number of cycles to blow a manual fuse, and can be reduced down to protect the system in the event of a faulty fuse.



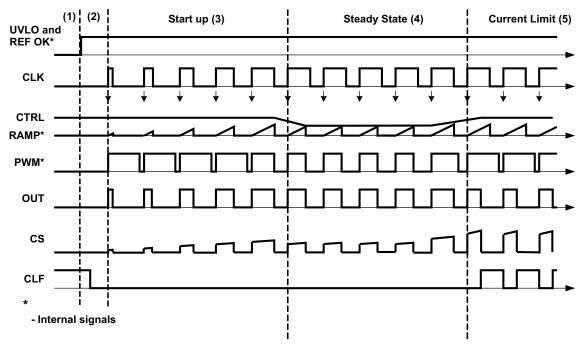
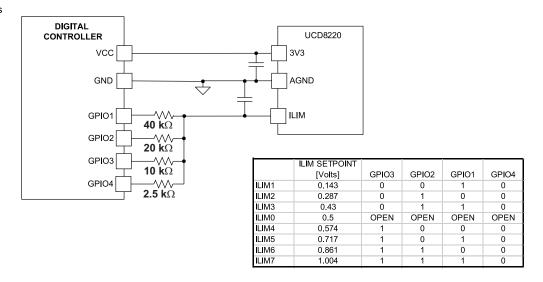


Figure 30. UCD8220 Timing and Circuit Operation Diagram

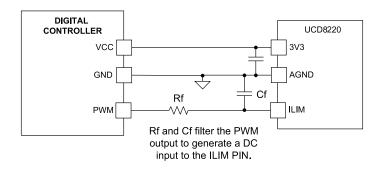


# **Current Sensing and Protection**

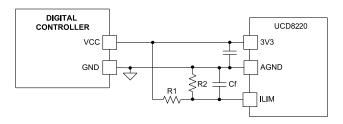
a) GPIO outputs



b) PWM output



c) Resistor divider



d) internal set point

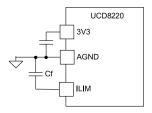


Figure 31. ILIM Settings



# Selecting the ISET Resistor for Voltage Mode Control

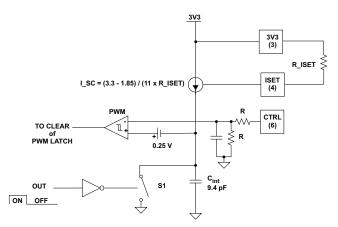


Figure 32. UCD8220 Configured in Voltage Mode Control with an Internal Timing Capacitor

When the ISET resistor is configured as shown in Figure 32 with the ISET resistor connected between the ISET pin and the 3V3 pin, the device is set-up for voltage mode control. For purposes of voltage loop compensation the, voltage ramp is 1.4 V from the valley to the peak. See Equation 1 for selecting the proper resistance for a desired clock frequency.

$$R_{ISET} = \frac{(3.3 - 1.85) \times 10^{12}}{11 \times 1.4 \times fclk \times 9.4} \Omega$$
 (1)

Where:

fclk = Desired Clock Frequency in Hz.

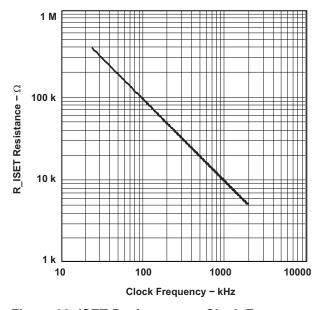


Figure 33. ISET Resistance vs Clock Frequency

Figure 33 shows the nominal value of resistance to use for a desired clock frequency. Note that for the UCD8220, which has two outputs controlled by Push-Pull logic, the output ripple frequency is equal to the clock frequency; and each output switches at half the clock frequency.

# Selecting the ISET Resistor for Voltage Mode Control with Voltage Feed forward

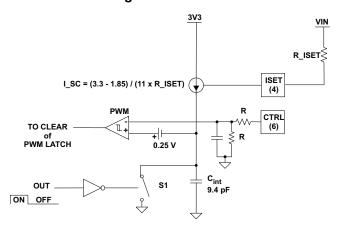


Figure 34. UCD8220 Configured in Voltage Mode Control with Voltage Feed Forward

When the ISET resistor is configured as shown in Figure 34 with the ISET resistor connected between the ISET pin and the input voltage, VIN, the device is configured for voltage mode control with voltage feed forward. For the purposes of voltage loop compensation, the voltage ramp is 1.4 x Vin/Vin\_max Volts from the valley to the peak. See Equation 2 for selecting the proper resistance for a desired clock frequency and input voltage range.

$$R_{ISET} = \frac{(Vin_{max} - 1.85) \times 10^{12}}{11 \times 1.4 \times fclk \times 9.4} \Omega$$
 (2)

Where:

fclk = Desired Clock Frequency in Hz.

For a general discussion of the benefits of Voltage Mode Control with Voltage feed forward, see Reference [5].



### Selecting the ISET Resistor for Peak Current Mode Control with Internal Slope Compensation

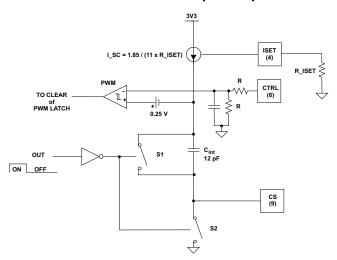


Figure 35. UCCD8220 Configured in Peak Current Control with Internal Slope Compensation

When the ISET resistor is configured as shown in Figure 35 with the ISET resistor connected between the ISET pin and AGND, the device is configured for peak current mode control with internal slope compensation. The voltage at the ISET pin is 1.85 volts so the internal slope compensation current, I\_SC, being fed into the internal slope compensation capacitor is equal to 1.85 / (11x R\_ISET). The voltage slope at the PWM comparator input which is generated by this current is equal to:

SLOPE = 
$$\frac{1.85 \times 10^6}{11 \times R_{\perp}ISET \times 12} V/\mu s$$
 (3)

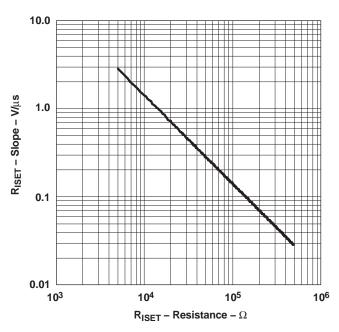


Figure 36. Slope vs RISET Resistance

The amount of slope compensation required depends on the design of the power stage and the output specifications. A general rule is to add an up-slope equal to the down slope of the output inductor. Refer to References 6 and 7 for a more detailed discussion regarding slope compensation in peak current mode controlled pwer stages.

# Handshaking

The UCD8220 has a built-in handshaking feature to facilitate efficient start-up of the digitally managed power supply. At start-up the CLF flag is held high until all the internal and external supply voltages of the UCD8220 is within its operating range. Once the supply voltages are within acceptable limits, the CLF goes low and the device processes the CLK signals. The digital controller should monitor the CFL flag at start-up and wait for the CLF flag to go LOW before sending CLK pulses to the UCD8K device.

### **Driver Output**

The high-current output stage of the UCD8220 is capable of supplying 4-A peak current pulses and swings to both PVDD and PGND.

The drive output uses the Texas Instruments TrueDrive™ architecture, which delivers rated current into the gate of a MOSFET when it is most needed, during the Miller plateau region of the switching transition providing efficiency gains.



TrueDrive<sup>™</sup> consists of pull-up/pull-down circuits with bipolar and MOSFET transistors in parallel. The peak output current rating is the combined current from the bipolar and MOSFET transistors. This hybrid output stage also allows efficient current sourcing at low supply voltages.

### Source/Sink Capabilities During Miller Plateau

Large power MOSFETs present a large load to the control circuitry. Proper drive is required for efficient, reliable operation. The UCD8220 driver has been optimized to provide maximum drive to a power MOSFET during the Miller plateau region of the switching transition. This interval occurs while the drain voltage is swinging between the voltage levels dictated by the power topology, requiring the charging/discharging of the drain-gate capacitance with current supplied or removed by the driver device. See Reference [2].

### **Drive Current and Power Requirements**

The UCD8220 contains drivers which can deliver high current into a MOSFET gate for a period of several hundred nanoseconds. High-peak current is required to turn on a MOSFET. Then, to turn off a MOSFET, the driver is required to sink a similar amount of current to ground. This repeats at the operating frequency of the power device.

Reference [2] discusses the current required to drive a power MOSFET and other capacitive-input switching devices.

When a driver device is tested with a discrete, capacitive load it is a fairly simple matter to calculate the power that is required from the bias supply. The energy that must be transferred from the bias supply to charge the capacitor is given by:

$$E = \frac{1}{2} \times CV^2 \tag{4}$$

where C is the load capacitor and V is the bias voltage feeding the driver.

There is an equal amount of energy transferred to ground when the capacitor is discharged. This leads to a power loss given by the following:

$$P = CV^2 \times f$$
 (5)

where f is the switching frequency.

This power is dissipated in the resistive elements of the circuit. Thus, with no external resistor between the driver and gate, this power is dissipated inside the driver. Half of the total power is dissipated when the capacitor is charged, and the other half is dissipated when the capacitor is discharged. With  $V_{DD}$  = 12 V,  $C_{LOAD}$  = 2.2 nF, and f = 300 kHz, the power loss can be calculated as:

$$P = 2.2 \text{ nF } \text{ x } 12^2 \text{ x } 300 \text{ kHz} = 0.095 \text{ W}$$
 (6)

With a 12-V supply, this would equate to a current of:

$$I = \frac{P}{V} = \frac{0.095 \text{ W}}{12 \text{ V}} = 7.9 \text{ mA}$$
 (7)

### Thermal Information

The useful range of a driver is greatly affected by the drive power requirements of the load and the thermal characteristics of the device package. In order for a power driver to be useful over a particular temperature range the package must allow for the efficient removal of the heat produced while keeping the junction temperature within rated limits. The UCD8220 is available in PowerPAD™ TSSOP and QFN/DFN packages to cover a range of application requirements. Both have an exposed pad to enhance thermal conductivity from the semiconductor junction.

As illustrated in Reference [3], the PowerPAD<sup>TM</sup> packages offer a leadframe die pad that is exposed at the base of the package. This pad is soldered to the copper on the PC board (PCB) directly underneath the device package, reducing the  $\theta_{JA}$  down to 37.47C/W. The PC board must be designed with thermal lands and thermal vias to complete the heat removal subsystem, as summarized in Reference [4].

Note that the PowerPAD™ is not directly connected to any leads of the package. However, it is electrically and thermally connected to the substrate which is the ground of the device. The PowerPAD™ should be connected to the quiet ground of the circuit.

### Circuit Layout Recommendations

In a MOSFET driver operating at high frequency, it is critical to minimize stray inductance to minimize overshoot/undershoot and ringing. The low output impedance of the drivers produces waveforms with high di/dt. This tends to induce ringing in the parasitic inductances. It is advantageous to connect the driver device close to the MOSFETs. It is recommended that the PGND and the AGND pins be connected to the PowerPAD™ of the package with a thin trace. It is critical to ensure that the voltage potential between these two pins does not exceed 0.3 V. The use of schottky diodes on the outputs to PGND and PVDD is recommended when driving gate transformers. See Reference 4 for a description of proper pad layout for the PowerPad® package.



### **REFERENCES**

- Power Supply Seminar SEM-1600 Topic 6: A Practical Introduction to Digital Power Supply Control, by Laszlo Balogh, Texas Instruments Literature No. SLUP224
- 2. Power Supply Seminar SEM-1400 Topic 2: Design And Application Guide For High Speed MOSFET Gate Drive Circuits, by Laszlo Balogh, Texas Instruments Literature No. SLUP133.
- 3. Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002
- 4. Application Brief, PowerPAD™ Made Easy, Texas Instruments Literature No. SLMA004
- 5. Power Supply Seminar SEM-300 Topic 2, "Closing the Feedback Loop", by Lloyd Dixon Jr., Texas Instruments, (Literature Number SLUP068)
- 6. Application Note, "Practical Considerations in Current Mode Power Supplies", Texas Instruments Literature Number SLUA110.
- 7. U-97, Application Note, Modelling, Analysis and Compensation of the Current-Mode Converter, Texas Instruments Literature Number SLUA101.

### **RELATED PRODUCTS**

PRODUCT	DESCRIPTION	FEATURES
UCD9501	Digital Power Controller for High Performance Multi-loop Applications	
MSP430F1232	Microcontroller	

### **REVISION HISTORY**

DATE	REVISION	CHANGE DESCRIPTION
03/05	SLUS652	Initial release.
08/05	SLUS652A	Extensive changes throughout
09/05	SLUS652B	Extensive changes throughout





com 1-Sep-2008

### **PACKAGING INFORMATION**

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
UCD8220PWP	ACTIVE	HTSSOP	PWP	16	90	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
UCD8220PWPG4	ACTIVE	HTSSOP	PWP	16	90	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
UCD8220PWPR	ACTIVE	HTSSOP	PWP	16	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
UCD8220PWPRG4	ACTIVE	HTSSOP	PWP	16	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR
UCD8220RSA	PREVIEW	QFN	RSA	16		TBD	Call TI	Call TI
UCD8220RSAR	PREVIEW	QFN	RSA	16		TBD	Call TI	Call TI

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

**Pb-Free** (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

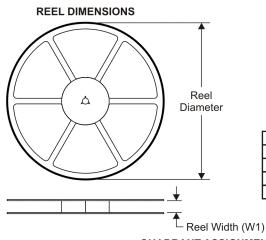
(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

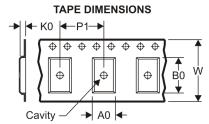
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# TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

# QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



# \*All dimensions are nominal

Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
UCD8220PWPR	HTSSOP	PWP	16	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1



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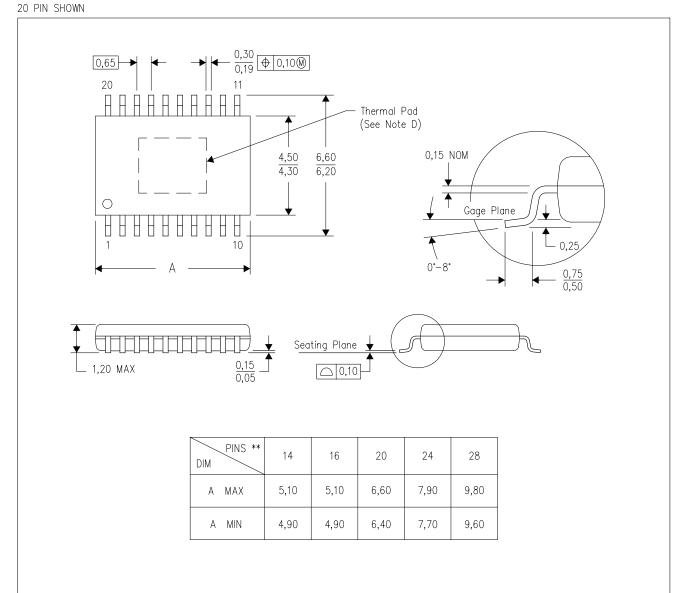


### \*All dimensions are nominal

	Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
I	UCD8220PWPR	HTSSOP	PWP	16	2000	346.0	346.0	29.0

4073225/H 12/05

PWP (R-PDSO-G\*\*) PowerPAD™ PLASTIC SMALL-OUTLINE PACKAGE



NOTES:

- All linear dimensions are in millimeters.
- This drawing is subject to change without notice.
- Body dimensions do not include mold flash or protrusions. Mold flash and protrusion shall not exceed 0.15 per side.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>>.
- E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.



# PWP (R-PDSO-G16)

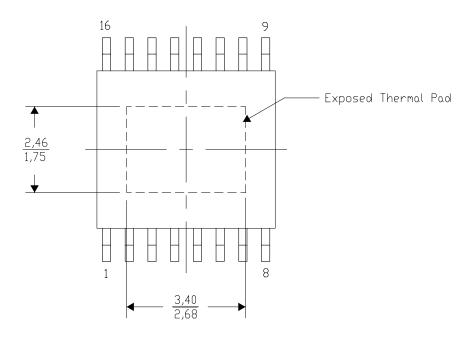
# PowerPAD™ SMALL PLASTIC DUTLINE

### THERMAL INFORMATION

This PowerPAD™ package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



Top View

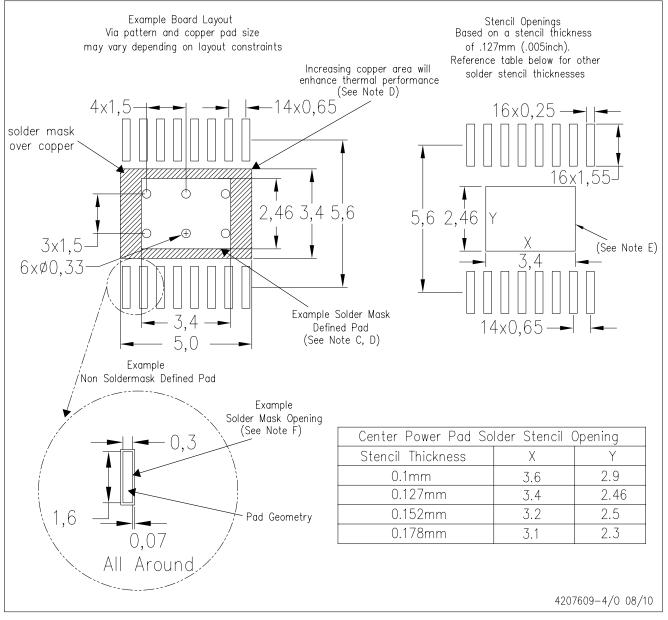
Exposed Thermal Pad Dimensions

4206332-4/R 08/10

NOTE: A. All linear dimensions are in millimeters

# PWP (R-PDSO-G16)

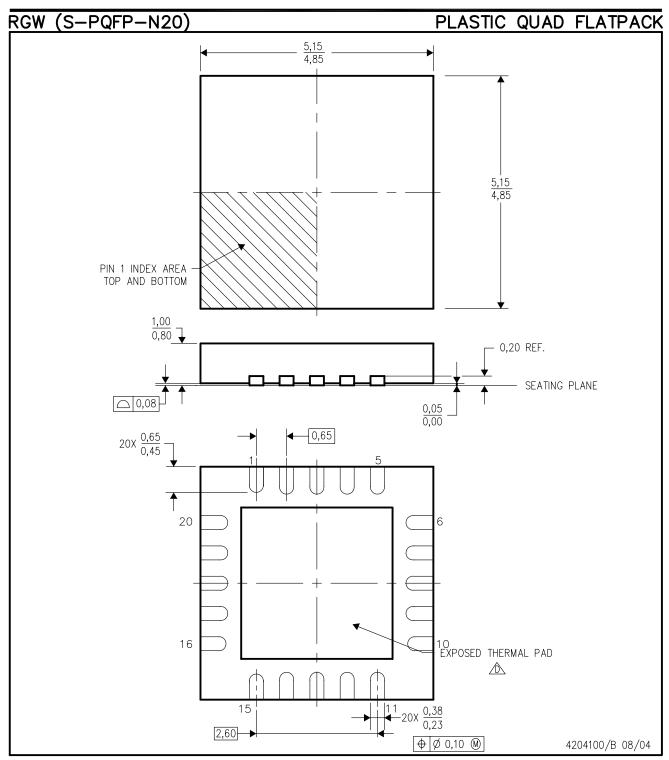
# PowerPAD™ PLASTIC SMALL OUTLINE



NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
- F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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- NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5—1994.
  - B. This drawing is subject to change without notice.
  - C. Quad Flat pack, No-leads (QFN) package configuration
  - The package thermal pad must be soldered to the board for thermal and mechanical performance..
    - See the Product Data Sheet for details regarding the exposed thermal pad dimensions.
  - E. Falls within JEDEC MO-220.



# RSA (S-PQFP-N16) PLASTIC QUAD FLATPACK 4,15 3,85 4,15 3,85 PIN 1 INDEX AREA TOP AND BOTTOM 0,80 0,20 REF. SEATING PLANE $\frac{0.05}{0.00}$ 0,08 $16X \frac{0,50}{0,30}$ 0,65 16 13 EXPOSED THERMAL PAD ⊕ Ø 0,10 M 4205141/B 11/04

- NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  - C. Quad Flatpack, No-leads (QFN) package configuration.
  - The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.
  - E. Falls within JEDEC MO-220.



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