### 1.2GHz to 2.7 GHz Direct IQ Modulator and Mixer

## feATURES

- Single 1.8 V to 5.25 V Supply
- Direct IQ Modulator with Integrated $90^{\circ}$ Phase Shifter*
- Four Step RF Power Control
- 120MHz Modulation Bandwidth
- Independent Double-Balanced Mixer
- Modulation Accuracy Insensitive to Carrier Input Power
- Modulator I/Q Inputs Internally Biased
- Available in 20-Lead FE Package


## APPLICATIOOS

- IEEE 802.11 DSSS and FHSS
- High Speed Wireless LAN (WLAN)
- Wireless Local Loop (WLL)
- PCS Wireless Data
- MMDS
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## DESCRIPTION

The $\mathrm{LT}^{\circledR} 5503$ is a front-end transmitter IC designed for low voltage operation. The IC contains ahigh frequency quadrature modulator with a variable gain amplifier (VGA) and a balanced mixer. The modulator includes a precision $90^{\circ}$ phase shifter which allows direct modulation of an RF signal by the baseband I and $Q$ signals.

In a superheterodyne system, the mixer can be used to generate the high-frequency RF input for the modulator by mixing the system's 1st and 2nd local oscillators.

The LT5503 modulator output P 1 dB is -3 dBm at 2.5 GHz . The VGA allows output power reduction in three steps up to 13 dB with digital control. The baseband inputs are internally biased for maximum input voltage swing at low supply voltage. If needed, they can be driven with external bias voltages.

## TYPICAL APPLICATION

2.45GHz Transmitter Application, Carrier for Modulator Generated by Upmixer



5503 G04
ABSOLUTE MAXIMUM RATINGS(Note 1)
Supply Voltage ..... 5.5V
Control Voltages

$\qquad$
-0.3 V to $\left(\mathrm{V}_{C C}+0.3 \mathrm{~V}\right)$
Baseband Voltages ( $\mathrm{BI}^{+}$to $\mathrm{Bl}^{-}$and $\mathrm{BQ}^{+}$to $\mathrm{BQ}^{-}$) ..... $\pm 2 \mathrm{~V}$
Baseband Common Mode Voltage .1 V to $\left(\mathrm{V}_{\mathrm{CC}}-\right.$ ..... 0.3 V
L01 Input Power ..... 4dBm
LO2 Input Power ..... 4dBm
MODIN Input Power ..... 4dBm
Operating Temperature Range

$\qquad$
$-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Storage Temperature Range $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Lead Temperature (Soldering, 10 sec )

$\qquad$

## ORDER INFORMATION

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING | PACKAGE DESCRIPTION | TEMPERATURE RANGE |
| :--- | :--- | :--- | :--- | :--- |
| LT5503EFE\#PBF | LT5503EFE\#TRPBF | 5503 | $20-$ Lead Plastic TSSOP | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ |

Consult LTC Marketing for parts specified with wider operating temperature ranges.
Consult LTC Marketing for information on nonstandard lead based finish parts.
For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

## ELECTRICAL CHARACTERISTICS (//a modulator)

$\mathrm{V}_{\mathrm{CC1} 1}=3 \mathrm{VDC}, 2.4 \mathrm{GHz}$ matching, MODEN $=$ High, $\mathrm{GC1}=\mathrm{GC2}=\mathrm{Low}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, MODRFIN $=2.45 \mathrm{GHz}$ at $-16 \mathrm{dBm},\left[\mathrm{I}-\mathrm{I}_{\mathrm{B}}\right]$ and $\left[\mathrm{Q}-\mathrm{Q}_{\mathrm{B}}\right]=$ 100 kHz CW signal at $1 V_{\text {p-p }}$ differential, Q leads I by $90^{\circ}$, unless otherwise noted. (Test circuit shown in Figure 2.) (Note 3 )

| PARAMETER | CONDITIONS | MIN TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: |
| RF Carrier Input (MODRFIN) |  |  |  |  |
| Frequency Range ${ }^{2}$ | Requires Appropriate Matching | 1.2 to 2.7 |  | GHz |
| Input VSWR | $Z_{0}=50 \Omega$ | 1.3:1 |  |  |
| Input Power |  | -20 to -10 |  | dBm |
| Baseband Inputs ( $\mathrm{Bl}^{+}, \mathrm{BI}^{-}, \mathrm{Ba}^{+}, \mathrm{BQ}^{-}$) |  |  |  |  |
| Frequency Bandwidth (3dB) |  | 120 |  | MHz |
| Differential Input Voltage for 1dB Compressed Output |  | 1 |  | $V_{\text {P-P }}$ |
| DC Common-Mode Voltage | Internally Biased | 1.4 |  | VDC |
| Differential Input Resistance |  | 18 |  | k $\Omega$ |
| Input Capacitance |  | 0.8 |  | pF |
| Gain Error |  | $\pm 0.2$ |  | dB |
| Phase Error |  | $\pm 1$ |  | DEG |

## Modulated RF Carrier Output (MODRFOUT)

| Output Power, Max Gain |  | -6 | -3 |
| :--- | :--- | :---: | :---: |
| Output VSWR | $\mathrm{Z}_{0}=50 \Omega$ | dBm |  |
| Image Suppression |  | -26 | -34 |
| Carrier Suppression |  | -24 | -32 |
| Output 1dB Compression |  | -3 | dBC |
| Output 3rd Order Intercept | $\mathrm{f}_{\mathrm{l}}=100 \mathrm{kHz}, \mathrm{f}_{\mathrm{Q}}=120 \mathrm{kHz}$ | dBc |  |
| Output 2rd Order Intercept | $\mathrm{f}_{\mathrm{l}}=100 \mathrm{kHz}, \mathrm{f}_{\mathrm{Q}}=120 \mathrm{kHz}$ | 2 | dBm |
| Broadband Noise | 20 MHz Offset | dBm |  |

VGA Control Logic (GC2, GC1)

| Switching Time |  | 100 | ns |
| :--- | :--- | :---: | :---: |
| Input Current |  | 2 | $\mu \mathrm{AA}$ |
| Input Low Voltage |  | 0.4 | VDC |
| Input High Voltage |  | 1.7 | VDC |
| Output Power Attenuation | GC2 $=$ Low, GC1 $=$ High | 4.5 | dB |
| Output Power Attenuation | GC2 $=$ High, GC1 $=$ Low | 9 | dB |
| Output Power Attenuation | GC2 $=$ High, GC1 $=$ High | 13.5 | dB |

Modulator Enable (MODEN) Low = Off, High = On

| Turn ON/OFF Time |  | 1 | $\mu \mathrm{~S}$ |
| :--- | :--- | :--- | :---: |
| Input Current |  | 105 | $\mu \mathrm{~A}$ |
| Enable |  | $V_{C C}-0.4$ | VDC |
| Disable |  |  | 0.4 |

Modulator Power Supply Requirements

| Supply Voltage |  | 1.8 | 5.25 | VDC |
| :--- | :--- | :--- | :---: | :---: |
| Modulator Supply Current | MODEN = High | 29 | 38 | mA |
| Modulator Shutdown Current | MODEN $=$ Low |  | 50 | $\mu \mathrm{~A}$ |

## ELECTRICAL CHARACTERISTICS (mieer)

$V_{\text {CC2 }}=3 V D C, 2.4 \mathrm{GHz}$ matching, MIXEN $=$ High, DMODE $=$ Low (LO2 $\div 2$ mode), $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{LO2IN}=750 \mathrm{MHz}$ at $-18 \mathrm{dBm}, \mathrm{LO1IN}=$ 2075 MHz at -12 dBm . MIXRFOUT measured at 2450 MHz , unless otherwise noted. (Test circuit shown in Figure 2.) (Note 3)

| PARAMETER | CONDITIONS | MIN | UNITS |
| :---: | :---: | :---: | :---: |
| Mixer 2nd LO Input (LO2IN) |  |  |  |
| Frequency Range | Internally Matched |  | MHz |
| Input VSWR | $Z_{0}=50 \Omega$ |  |  |
| Input Power |  |  | dBm |
| Mixer 1st LO Input (LO1IN) |  |  |  |
| Frequency Range ${ }^{2}$ | Requires Appropriate Matching |  | MHz |
| Input VSWR | $Z_{0}=50 \Omega$ |  |  |
| Input 3rd Order Intercept | $-30 \mathrm{dBm} /$ Tone, $\Delta \mathrm{f}=200 \mathrm{kHz}$ |  | dBm |
| Mixer RF Output (MIXRFOUT) |  |  |  |
| Frequency Range ${ }^{2}$ | Requires Appropriate Matching |  | MHz |
| Output VSWR | $Z_{0}=50 \Omega$ |  |  |
| Small-Signal Conversion Gain | $\mathrm{P}_{\mathrm{L} 01}=-30 \mathrm{dBm}$ |  | dB |
| Output Power |  | -14.7 | dBm |
| L01 Suppression |  | -22 | dBC |
| Output 1dB Compression |  |  | dBm |
| Broadband Noise | 20MHz Offset |  | $\mathrm{dBm} / \mathrm{Hz}$ |

LO2 Divider Mode Control (DMODE) Low $=\mathrm{f}_{\mathrm{L} 02 \div 2} \div \mathrm{High}=\mathrm{f}_{\mathrm{L} 02 \div 1}$

| Input Current |  | 1 | $\mu \mathrm{~A}$ |
| :--- | :--- | :--- | ---: |
| Input Low Voltage $(\div 2)$ |  |  | 0.4 |
| Input High Voltage $(\div 1)$ |  | $V_{C C}-0.4$ | VDC |

Mixer Enable (MIXEN) Low = Off, High = On

| Turn ON/OFF Time |  | 1 |  |
| :--- | :--- | :--- | :---: |
| Input Current |  | 130 | $\mu \mathrm{~s}$ |
| Enable |  | $V_{\text {CC }}-0.4$ | $\mu \mathrm{~A}$ |
| Disable |  |  | VDC |

## Mixer Power Supply Requirements

| Supply Voltage |  | 1.8 | 5.25 | VDC |
| :--- | :--- | :--- | :---: | :---: |
| Supply Current ( $\div 2$ mode) | DMODE $=$ Low, MIXEN $=$ High | 11.9 | 15.5 | mA |
| Supply Current ( $\div 1$ mode) | DMODE $=$ High, MIXEN $=$ High | 10.8 | mA |  |
| Shutdown Current | MIXEN = Low |  | 10 | $\mu \mathrm{~A}$ |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Note 2: External component values on the final test circuit shown in Figure 2 are optimized for operation in the 2.4 GHz to 2.5 GHz band.
Note 3: Specifications over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ temperature range are assured by design, characterization and correlation with statistical process controls.

## TYPICAL PERFORMANCE CHARACTERISTICS (I/Q Modulator)

$V_{C C 1}=3 V D C, 2.4 \mathrm{GHz}$ matching, MODEN $=$ high, $\mathrm{GC1}=\mathrm{GC2}=$ low ( max gain), $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{MODRFIN}=2.45 \mathrm{GHz}$ at -16 dBm , $\left(1-I_{B}\right)$ and $\left(\mathrm{Q}-\mathrm{Q}_{\mathrm{B}}\right)=100 \mathrm{kHz}$ sine at $1 \mathrm{~V}_{\mathrm{P}-\mathrm{p}}$ differential, Q leads I by $90^{\circ}$, unless otherwise noted. (Test circuit shown in Figure 2.)


Typical SSB Spectrum


## TYPICAL PERFORMANCE CHARACTERISTICS (Ha moduluator

2.4 GHz matching, MODEN $=$ high, $\mathrm{GC1}=\mathrm{GC2}=\operatorname{low}\left(\max\right.$ gain), MODRFIN $=2.45 \mathrm{GHz},\left(\mathrm{I}-\mathrm{I}_{\mathrm{B}}\right)$ and $\left(\mathrm{O}-\mathrm{Q}_{\mathrm{B}}\right)=100 \mathrm{kHz}$ sine at $1 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ differential, Q leads I by $90^{\circ}$, unless otherwise noted. (Test circuit shown in Figure 2.)


## TYPICAL PERFORMAOCE CHARACTERISTICS (I/a modulator)

$V_{C C 1}=3 V D C$, MODEN $=$ high, $T_{A}=25^{\circ} \mathrm{C}, P_{\text {MODRFIN }}=-16 \mathrm{dBm},\left(I-I_{B}\right)$ and $\left(Q-Q_{B}\right)=100 \mathrm{kHz}$ sine at $1 V_{P-P}$ differential, $Q$ leads $I$ by $90^{\circ}$, unless otherwise noted. (Test circuit shown in Figure 2.)


## TYPICAL PERFORMANCE CHARACTERISTICS (Mixer)

2.4 GHz matching, MIXEN $=$ high, DMODE $=$ low ( $\mathrm{LO2} \div 2$ mode ), $\mathrm{LO} 2 \mathrm{IN}=750 \mathrm{MHz}$ at $-18 \mathrm{dBm}, \mathrm{LO1IN}=2075 \mathrm{MHz}$. MIXRFOUT measured at 2450MHz, unless otherwise noted. (Test circuit shown in Figure 2.)


## TYPICAL PGRFORMANCE CHARACTERISTICS (mixer)

$\mathrm{V}_{\text {CC2 }}=3 \mathrm{VDC}$, MIXEN $=$ high, DMODE $=$ low ( $\mathrm{LO2} \div 2$ mode), $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted. (Test circuit shown in Figure 2.)


MIXEN Input Current vs Enable Voltage (MIXEN = VCC2)


## PIn functions

BQ $^{-}$(Pin 1): Negative Baseband Input Pin of the Modulator Q-Channel. This pin is internally biased to 1.4 V , but can also be overdriven with an external $D C$ voltage greater than 1.4 V , but less than $\mathrm{V}_{\mathrm{CC}}-0.4 \mathrm{~V}$.
$\mathbf{B Q}^{+}$(Pin 2): Positive Baseband Input Pin of Modulator QChannel. This pin is internally biased to 1.4 V , but can also be overdriven with an external DC voltage greater than 1.4 V , but less than $\mathrm{V}_{\mathrm{CC}}-0.4 \mathrm{~V}$.

GC1 (Pin 3): Gain Control Pin. This pin is the least significant bit of the four-step modulator gain control.
MODIN (Pin 4): Modulator Carrier Input Pin. This pin is internally biased and should be AC-coupled. An external matching network is required for a $50 \Omega$ source.
VCCMOD (Pin 5): Power Supply Pin for the I/Q Modulator. This pin should be externally connected to the other $V_{C C}$ pins and decoupled with 1000 pF and $0.1 \mu \mathrm{~F}$ capacitors.
$\mathbf{V}_{\text {cc }}$ RF (Pin 6): Power Supply Pin for the I/Q Modulator Input RF Buffer and Phase Shifter. This pin should be externally connected to the other $V_{C C}$ pins and decoupled with 1000 pF and $0.1 \mu \mathrm{~F}$ capacitors.
L01 (Pin 7): Mixer 1st LO Input Pin. This pin is internally biased and should be AC-coupled. An external matching network is required for a $50 \Omega$ source.
VCcL01 (Pin 8): Power Supply Pin for the Mixer L01 Circuits. This pin should be externally connected to the other $V_{\text {CC }}$ pins and decoupled with 1000 pF and $0.1 \mu \mathrm{~F}$ capacitors.

DMODE (Pin 9): Mixer 2nd LO Divider Mode Control Pin. Low = divide-by-2, High = divide-by-1.
MX ${ }^{+}$(Pin 10): Mixer Positive RF Output Pin. This pin must be connected to $\bigvee_{\text {CC }}$ through an external matching network.

MX́ (Pin 11): Mixer Negative RF Output Pin. This pin must be connected to $\bigvee_{\text {CC }}$ through an external matching network.

MIXEN (Pin 12): Mixer Enable Pin. When the input voltage is higher than $\mathrm{V}_{C C}-0.4 \mathrm{~V}$, the mixer circuits supplied through pins $8,10,11$ and 15 are enabled. When the input voltage is less than 0.4 V , these circuits are disabled.
MODEN (Pin 13): Modulator Enable Pin. When the input voltage is higher than $\mathrm{V}_{\mathrm{CC}}-0.4 \mathrm{~V}$, the modulator circuits supplied through pins 5, 6, 16 and 17 are enabled. When the input voltage is less than 0.4 V , these circuits are disabled.
LO2 (Pin 14): Mixer 2nd LO Input Pin. This pin is internally biased and should be AC-coupled. An external matching network is not required, but can be used for improved matching to a $50 \Omega$ source.
$V_{\text {CcLO2 }}$ (Pin 15): Power Supply Pin for the Mixer L02 Circuits. This pin should be externally connected to the other $V_{C C}$ pins and decoupled with 1000 pF and $0.1 \mu \mathrm{~F}$ capacitors.
$V_{\text {cc }}$ VGA (Pin 16): Power Supply Pin for the Modulator Variable Gain Amplifier. This pin should be externally connected to the other $V_{\text {CC }}$ pins through a $47 \Omega$ resistor and decoupled with a good high frequency capacitor (2pF typical) placed close to the pin.
MODOUT (Pin 17): Modulator RF Output Pin. This pin must be externally biased to $\mathrm{V}_{\text {Cc }}$ through a bias choke. An external matching network is required to match to $50 \Omega$.
GC2 (Pin 18): Gain Control Pin. This pin is the most significant bit of the four-step modulator gain control.
$\mathrm{BI}^{+}($Pin 19): Positive Baseband Input Pin of the Modulator I-Channel. This pin is internally biased to 1.4 V , but can also be overdriven with an external DC voltage greater than 1.4 V , but less than $\mathrm{V}_{C C}-0.4 \mathrm{~V}$.
$\mathbf{B I}^{-}$(Pin 20): Negative Baseband Input Pin of the Modulator I-Channel. This pin is internally biased to 1.4 V , but can also be overdriven with an external DC voltage greater than 1.4 V , but less than $\mathrm{V}_{C C}-0.4 \mathrm{~V}$.

Exposed Pad (Pin 21): Circuit Ground Return for the Entire IC. This must be soldered to the printed circuit board ground plane

## BLOCK DIAGRAM



| Application Dependent Component Values |  |  |  |
| :--- | :---: | :---: | :---: |
|  | $\mathbf{1 . 2 G H z}$ Matching <br> (Modulator Only) | $\mathbf{1 . 9 G H z}$ Matching | 2.4GHz Matching |
| L1 | 33 nH | 22 nH | 18 nH |
| L2 | 12 nH | 5.6 nH | 2.7 nH |
| L3 | 12 nH | 4.7 nH | 2.7 nH |
| C2, C3, C7 | 39 pF | 15 pF | 8.2 pF |
| C10 | 2.7 pF | 1.8 pF | 1.2 pF |
| C23 | $\mathrm{n} / \mathrm{a}$ | 1.5 pF | 1.5 pF |
| R1 | $240 \Omega$ | $390 \Omega$ | $390 \Omega$ |
| C 4 | $\mathrm{n} / \mathrm{a}$ | 15 pF | 8.2 pF |
| $\mathrm{C} 5, \mathrm{C} 6$ | $\mathrm{n} / \mathrm{a}$ | 1.8 pF | 2.2 pF |
| C 9 | $\mathrm{n} / \mathrm{a}$ | 15 pF | 2.7 pF |
| C 11 | $\mathrm{n} / \mathrm{a}$ | 2.2 pF | 1.2 pF |
| L4 | $\mathrm{n} / \mathrm{a}$ | 6.8 nH | 4.7 nH |
| L5,L6 | $\mathrm{n} / \mathrm{a}$ | 5.6 nH | 2.2 nH |
| T1 | $\mathrm{n} / \mathrm{a}$ | LDB211G9010C-001 | LDB212G4005C-001 |

Figure 1. Test Schematic for 1.2GHz, 1.9GHz and 2.4GHz Applications

## APPLICATIONS INFORMATION

The LT5503 consists of a direct quadrature modulator and a mixer. The mixer operates over the range of 1.7 GHz to 2.7 GHz , and the modulator operates with an output range of 1.2 GHz to 2.7 GHz . The LT5503 is designed specifically for high accuracy digital modulation with supply voltages as low as 1.8 V . It is suitable for IEEE 802.11b wireless local area network (WLAN), MMDS and wireless local loop (WLL) transmitters.
A dual-conversion RF system requires two local oscillators to convert signals between the baseband and RF domains (see Figure 2). The LT5503's double-balanced mixer can be used to generate the LT5503 modulator's high frequency carrier input (MODRFIN) by mixing the systems 1st and 2nd local oscillators (LO1 and LO2). In this case, a bandpass filter is required to select the desired mixer output for the modulator input. The mixer's RF differential output produces -12 dBm typically at 2.45 GHz and the modulator MODIN pin requires $\geq-16 \mathrm{dBm}$, driven single-ended. This allows approximately 4dB margin for
bandpass filter loss. The balanced output from the modulator is applied to a variable gain amplifier (VGA) that provides a single-ended output. Note that the modulator can also be used independently of the mixer, freeing the mixer to be used anywhere in the system. In this case, MODRFIN will be driven from an external frequency source.

## Modulator Baseband

The baseband I and Q inputs ( $\mathrm{BI}^{+} / \mathrm{BI}^{-}$and $\mathrm{BQ}^{+} / \mathrm{BQ}^{-}$) are internally biased to 1.4 V to maximize the input signal range at low supply voltage. This bias voltage is stable over temperature, and increases by approximately 50 mV at the maximum supply voltage. The modulator I and $Q$ inputs have very wide bandwidth (120MHz typical), making the LT5503 suitable for even the most wideband modulation applications. For best carrier suppression and lowest distortion, differential input drive should be used. Singleended drive is possible too, with the unused inputs ACcoupled to ground.


Figure 2. Example System Block Diagram for a Dual Conversion System

## APPLICATIONS InFORMATION

AC-Coupled Baseband. Figure 3 shows the simplified circuit schematic of a high-pass AC-coupled baseband interface.


Figure 3. AC-Coupled Baseband Interface
With approximately 18k of differential input resistance, the suggested minimum AC-coupling capacitor can be determined using the following equation:

$$
\mathrm{C}_{\mathrm{CPL}}=\frac{1}{\left(18 \cdot 10^{3} \cdot \pi \bullet \mathrm{f}_{\mathrm{C}}\right)}
$$

where $f_{c}$ is the 3 dB cut-off frequency of the baseband input signal.
A larger capacitor may be used where the settling time of charging and discharging the AC-coupling capacitor is not critical.

DC-Coupled Baseband. The baseband inputs' internal bias voltage can be overdriven with an external bias circuit. This facilitates direct interfacing to a D/A converter for faster transient response. In this case, the LT5503's baseband inputs are DC biased by the converter. The optimal $\mathrm{V}_{\text {BIAS }}$ is 1.4 V , independent of $\mathrm{V}_{C C}$. In general, the maximum $\mathrm{V}_{\text {BIAS }}$ should be less than $\mathrm{V}_{\mathrm{CC}}-0.4 \mathrm{~V}$. The DC load on each converter output can be approximated using the following equation where $\mathrm{l}_{\text {INPUT }}$ is the current flowing into a modulator input:

$$
\mathrm{I}_{\mathrm{INPUT}}=\frac{\mathrm{V}_{\mathrm{BIAS}}-1.4 \mathrm{~V}}{9 \mathrm{k} \Omega}
$$

Figure 4 shows a simplified circuit schematic for interfacing the LT5503's baseband inputs to the outputs of a D/A converter. OIP and OIN are the positive and negative baseband outputs, respectively, of the converter's I-channel. Similarly, OQP and OQN are the positive and negative baseband outputs, respectively, of the converter's Q-channel.


Figure 4. DC-Coupled Baseband Interface

## Modulator RF Input (MODRFIN)

The modulator RF input buffer is driven single-ended. An internal active balun circuit produces balanced signals to drive the integrated phase shifter. Limiters following the phase shifter output accommodate a wide range of MODRFIN power, resulting in minimal degradation of modulation gain/phase accuracy performance or carrier feedthrough. This pin is easily matched to a $50 \Omega$ source with the simple lowpass network shown in Figure 1. This pin is internally biased, therefore an AC-coupling capacitor is required.

## Modulator VGA (Variable Gain Amp)

The VGA has two digital selection lines to provide a nominal $0 \mathrm{~dB}, 4.5 \mathrm{~dB}, 9 \mathrm{~dB}$ and 13.5 dB attenuation from the maximum modulator output power setting. The logic table is shown below:

| Attenuation |  | GC2 |  |
| :---: | :---: | :---: | :---: |
|  |  | Low | OdB |

## APPLICATIONS INFORMATION

Pin 16 should be connected externally to $V_{C C}$ through a low value series resistor ( $47 \Omega$ typical). To assure proper output power control, a good, local high frequency AC ground for Pin 16 is essential. The MODOUT port of the VGA is an open collector configuration. An inductor with high self resonance frequency is required to connect Pin 17 to $V_{\text {CC }}$ as a DC return path, and as a part of the output matching network. Additional matching components are required to drive a $50 \Omega$ load as shown in Figure 1. The amplifier is designed to operate in Class A for Iow distortion performance. The typical output 1dB compression point ( P 1 dB ) is -3 dBm at 2.45 GHz . When the differential baseband input voltages are higher than $1 V_{\text {P-p }}$, the VGA operates in Class AB mode, and the distortion performance of the modulator is degraded. The logic control inputs do not draw current when they are low. They draw about $2 \mu A$ each when high.

## Mixer L01 Port

The mixer L01 input port is the linear input to the mixer. It consists of an active balun amplifier designed to operate over the 1.4 GHz to 2.4 GHz frequency range. There is a linear relationship between L01 input power and MIXRFOUT power for L01 input levels up to approximately -20 dBm . After that, the mixer output begins to compress. When operated in the recommended -14 dBm to -8 dBm input power range, the mixer is well compressed, which in turn creates a stable output level for the modulator input. As shown in Figure 1, a simple lowpass matching network is required to match this pin to $50 \Omega$. This pin is internally biased, therefore an AC-coupling capacitor is required.


Figure 5. $50 \Omega$ Mixer Output Matching Without a Balun

|  | $\mathbf{1 . 9 G H z}$ | $\mathbf{2 . 4 G H z}$ |
| :--- | :---: | :---: |
| $\mathrm{L} 5, \mathrm{~L} 6$ | 5.6 nH | 2.7 nH |
| $\mathrm{C}, \mathrm{C} 6$ | 1.8 pF | 0.68 pF |
| C 9 | 15 pF | 8.2 pF |

## Mixer L02 Port

The mixer LO2 port is designed to operate in the 50MHz to 1000 MHz range. The first stage is a limiting amplifier. This stage produces the correct output levels to drive the internal divider circuit reliably, with L02 input levels down to -20 dBm . The output of the divider then drives another stage, which in turn switches the nonlinear inputs of the double-balanced mixer. Note that the mixer output will produce broadband noise if the LO2 signal level is too low. The input amplifier is designed for a good match over the entire frequency range. The only requirement (Figure 1) is an external AC-coupling capacitor.

## Mixer Output Ports (MX ${ }^{+} / \mathrm{MX}^{-}$)

The mixer output is a differential open collector configuration. Bias current is supplied to these two pins through the center tap of a balun as shown in Figure 1. Simple lowpass matching is used to transform each leg of the mixer output to $25 \Omega$ for the balun's $50 \Omega$ input impedance.

The balun approach provides the highest output power and best L01 suppression, but is not absolutely necessary. It is also possible to match each output to $50 \Omega$ and couple power from one output. The unused output should be terminated in the same characteristic impedance. In this case, output power is approximately 2 dB lower and L01 suppression degrades to approximately 15 dBc . A schematic for this approach is shown in Figure 6 where inductors $\mathrm{LB}^{+}$and $\mathrm{LB}^{-}$supply bias current to the mixer's differential outputs, and resistor RTERM terminates the unused output.

## APPLICATIONS INFORMATION

## EVALUATION BOARD

Figure 6 shows the circuit schematic of the evaluation board. The MODRFIN, MODRFOUT and MIXRFOUT ports are matched to $50 \Omega$ at 2.45 GHz . The LO1IN port is matched to $50 \Omega$ at 2.1 GHz and the LO2IN port is internally matched.

A $390 \Omega$ resistor is used to reduce the quality factor ( $Q$ ) of the modulator output and deliver an output power of -3 dBm typically. A lower value resistor may be used if the desired output power is lower. For example, the output power will be 3 dB lower if a $200 \Omega$ resistor is used.
Inductors with high self-resonance frequency should be used for L1 to L6.

For simpler evaluation in a lab environment, the evaluation board includes op amps to convert single-ended I and Q input signals to differential . The op amp configuration has a voltage gain of two; therefore the peak baseband input voltage should be halved to maintain the same RF output power. The op amp configuration shown will maintain acceptable differential balance up to 10 MHz typically. It is also possible to bypass the op amps and drive the modulator's differential inputs directly by connecting to the four oversized vias on the board (V1, V2, V3 and V4).

Figure 6 also shows a table of matching network values for designs centered at 1.9 GHz and 1.2 GHz .
Figure 7 shows the evaluation board with connectors and ICs. Figure 8 shows the test set-up with the upconverting mixer and IQ modulator connected in a transmit configuration. Refer to the demo board DC365A Quick Start Guide for detailed testing information.

## RF Layout Tips:

- Use $50 \Omega$ impedance transmission lines up to the matching networks, use of a ground plane is a must.
- Keep the matching networks as close to the pins as possible.
- Surface mount 0402 outline (or smaller) parts are recommended to minimize parasitic inductances and capacitances.
- Isolate the MODOUT pin from the LO2 input by putting the LO2 transmission line on the bottom side of the board.
- The only ground connection is through the exposed pad on the bottom of the package. This exposed pad must be soldered to the board in such a way to get complete RF contact.
- Low impedance RF ground connections are essential and can only be obtained by one or more vias tying directly into the ground plane.
- $V_{C C}$ lines must be decoupled with low impedance, broadband capacitors to prevent instability.
- Separate power supply lines should be used to isolate the MODIN signal and other stray signals from the MODOUT line. If possible, power planes should be used.
- Avoid use of long traces whenever possible. Long RF traces in particular can lead to signal radiation and degraded isolation, as well as higher losses.


## APPLICATIONS INFORMATION



Figure 6. Evaluation Circuit Schematic for $1.2 \mathrm{GHz}, 1.9 \mathrm{GHz}$ and 2.4 GHz Applications
www.BDTIC.com/Linear

## LT5503

APPLICATIONS INFORMATION


Figure 7. LT5503 Evaluation Board Layout

## APPLICATIONS INFORMATION



Figure 8. Test Set-Up for Upconverting Mixer and I/Q Modulator Transmit Chain Measurements.

## PACKAGE DESCRIPTION

## FE Package

20-Lead Plastic TSSOP (4.4mm)
(Reference LTC DWG \# 05-08-1663)
Exposed Pad Variation CB


RECOMMENDED SOLDER PAD LAYOUT


NOTE:

1. CONTROLLING DIMENSION: MILLIMETERS 2. DIMENSIONS ARE IN MILLIMETERS
2. DRAWING NOT TO SCALE

$\begin{array}{llllllllll}1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 & 10\end{array}$

. RECOMMENDED MINIMUM PCB METAL SIZE FOR EXPOSED PAD ATTACHMENT
DIMENSIONS DO NOT INCLUDE MOLD FLASH. MOLD FLASH
SHALL NOT EXCEED 0.150 mm (.006") PER SIDE

## beLATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| LT5500 | RF Front End | Dual LNA Gain Setting $+13.5 \mathrm{~dB} /-14 \mathrm{~dB}$ at 2.5 GHz , Double-Balanced Mixer, $1.8 \mathrm{~V} \leq \mathrm{V}_{\text {SUPPLY }} \leq 5.25 \mathrm{~V}$ |
| LT5502 | 400MHz Quadrature Demodulator with RSSI | 1.8 V to 5.25V Supply, 70 MHz to 400MHz IF, 84dB Limiting Gain, 90dB RSSI Range |
| LT5504 | 800MHz to 2.7GHz RF Measuring Reciever | 80dB Dynamic Range, Temperature Compensated, 2.7V to 5.5V Supply |
| LT5505 | 300 MHz to 3.5GHz RF Power Detector | $>40 \mathrm{~dB}$ Dynamic Range, Temperature Compensated, 2.7V to 6V Supply |
| LT5506 | 500 MHz Quadrature IF Demodulator with VGA | 1.8 V to 5.25V Supply, 40MHz to 500MHz IF, -4 dB to 57dB Linear Power Gain |
| LTC5507 | 100kHz to 1GHz RF Power Detector | 48dB Dynamic Range, Temperature Compensated, 2.7V to 6V Supply |
| LTC5508 | 300MHz to 7GHz RF Power Detector | SC70 Package |
| LTC5509 | 300MHz to 3GHz RF Power Detector | 36dB Dynamic Range, SC70 Package |
| LT5511 | High Signal Level Up Converting Mixer | RF Output to 3GHz, 17dBm IIP3, Integrated LO Buffer |
| LT5512 | High Signal Level Down Converting Mixer | DC-3GHz, 20dBm IIP3, Integrated LO Buffer |
| LT5515 | 1.5GHz to 2.5GHz Direct Conversion Demodulator | 20 dBm IIP3, Integrated LO Quadrature Generator |
| LT5516 | 0.8 GHz to 1.5 GHz Direct Conversion Quadrature Demodulator | 21.5dBm IIP3, Integrated LO Quadrature Generator |
| LT5522 | 600MHz to 2.7GHz High Signal Level Mixer | 25 dBm IIP3 at 900 MHz , 21.5 dBm IIP3 at 1.9 GHz , Matched $50 \Omega \mathrm{RF}$ and LO Ports, Integrated LO Buffer |
| LTC5532 | 300MHz to 7GHz Precision RF Power Detector | Precision Vout Offset Control, Adjustable Gain and Offset Voltage |

