

### ESD immunity-level optimization of a high-side switch application based on the VNI4140K

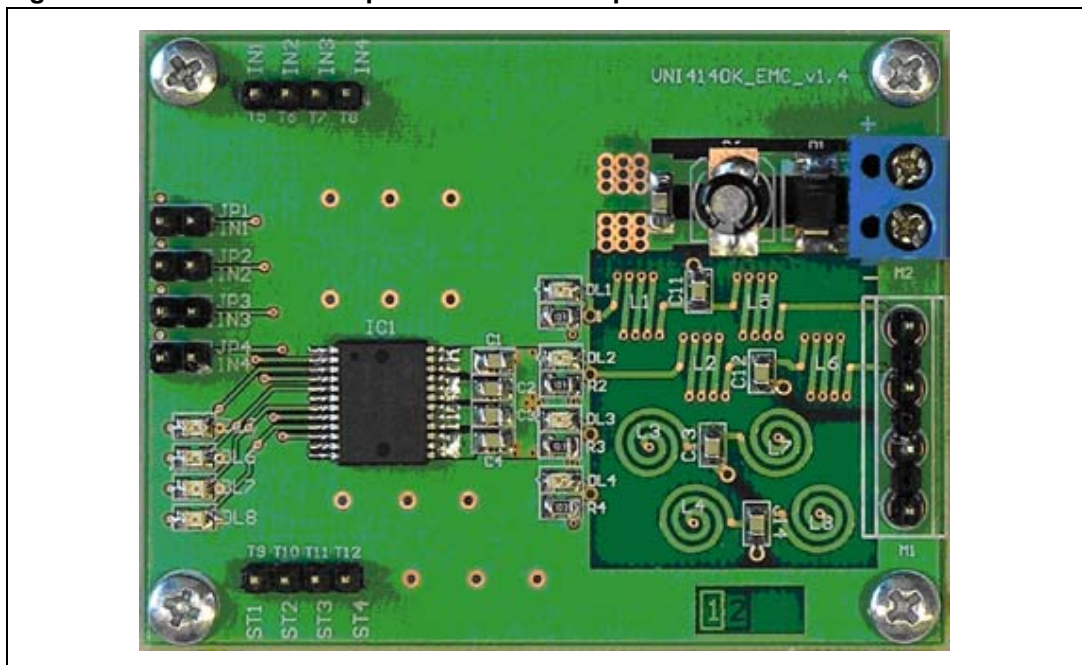
#### Introduction

The VNI4140K is a quad-channel high-side driver designed for industrial applications. It is a monolithic device manufactured using STMicroelectronics' most advanced VIPower® technology, intended for driving four independent resistive or inductive loads with one side connected to ground. The device fully complies with standards including JEDEC (JESD22) and IEC 61131-2. It conforms to the "human body model" ESD test in accordance with the JESD22-A114 definition. The immunity level is 2000 V, as stated in the datasheet of the device.

When the VNI4140K is mounted in the complete application, the system must meet minimum requirements defined by generic standard IEC 61000-4-2. However, the actual immunity level depends on the manufacturer of the final application. To achieve the required level of immunity, the device must be equipped with a suitable application environment, external components and/or a suitable PCB layout.

This application note provides some recommendations on how to optimize the ESD immunity level of the VNI4140K high-side switch application in accordance with the IEC 61000-4-2 standard.

**Figure 1. VNI4140K ESD optimized PCB example**



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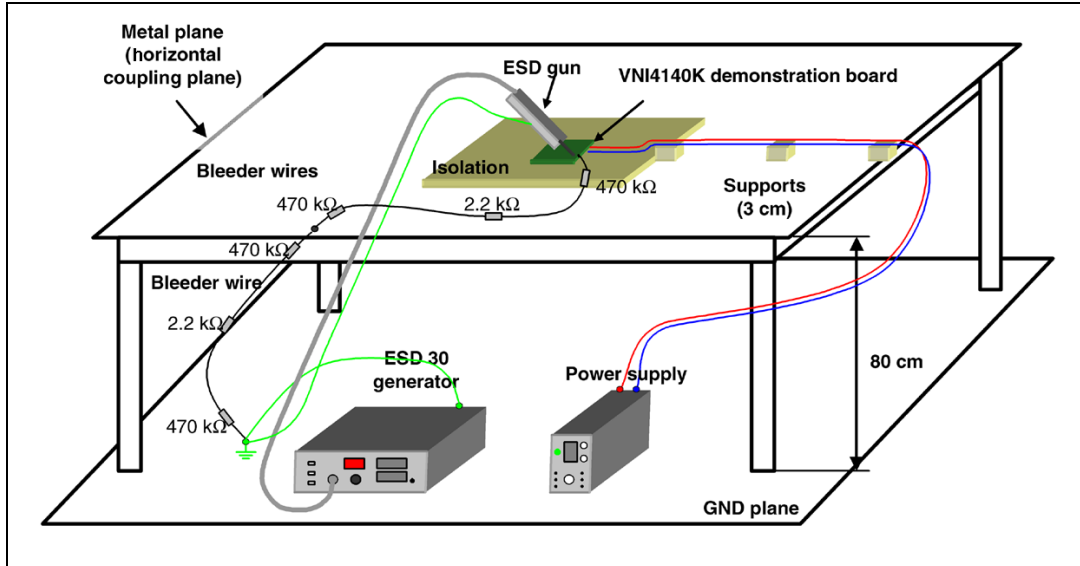
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## 2 Test setup according to IEC 61000-4-2

The IEC 61000-4-2 standard provides the test procedure for various types of applications. The test setup for ungrounded (tabletop) equipment is selected. The structure is shown in [Figure 2](#).

**Figure 2. ESD test setup according to IEC 61000-4-2**



### 2.1 Test conditions

- Supply voltage: 24 VDC, always ON
- Inputs OFF, outputs OFF
- Air discharge
- Polarity: positive/negative
- Discharge unit: 150 pF / 330 Ω
- Applied to: board output terminal

### 2.2 Classification of the test

- A** - normal performance
- B** - temporary degradation or loss of function or performance, with automatic return to normal operation
- C** - temporary degradation or loss of function which requires external intervention to recover normal operation
- D** - degradation or loss of function, need substitution of damaged components to recover normal operation.

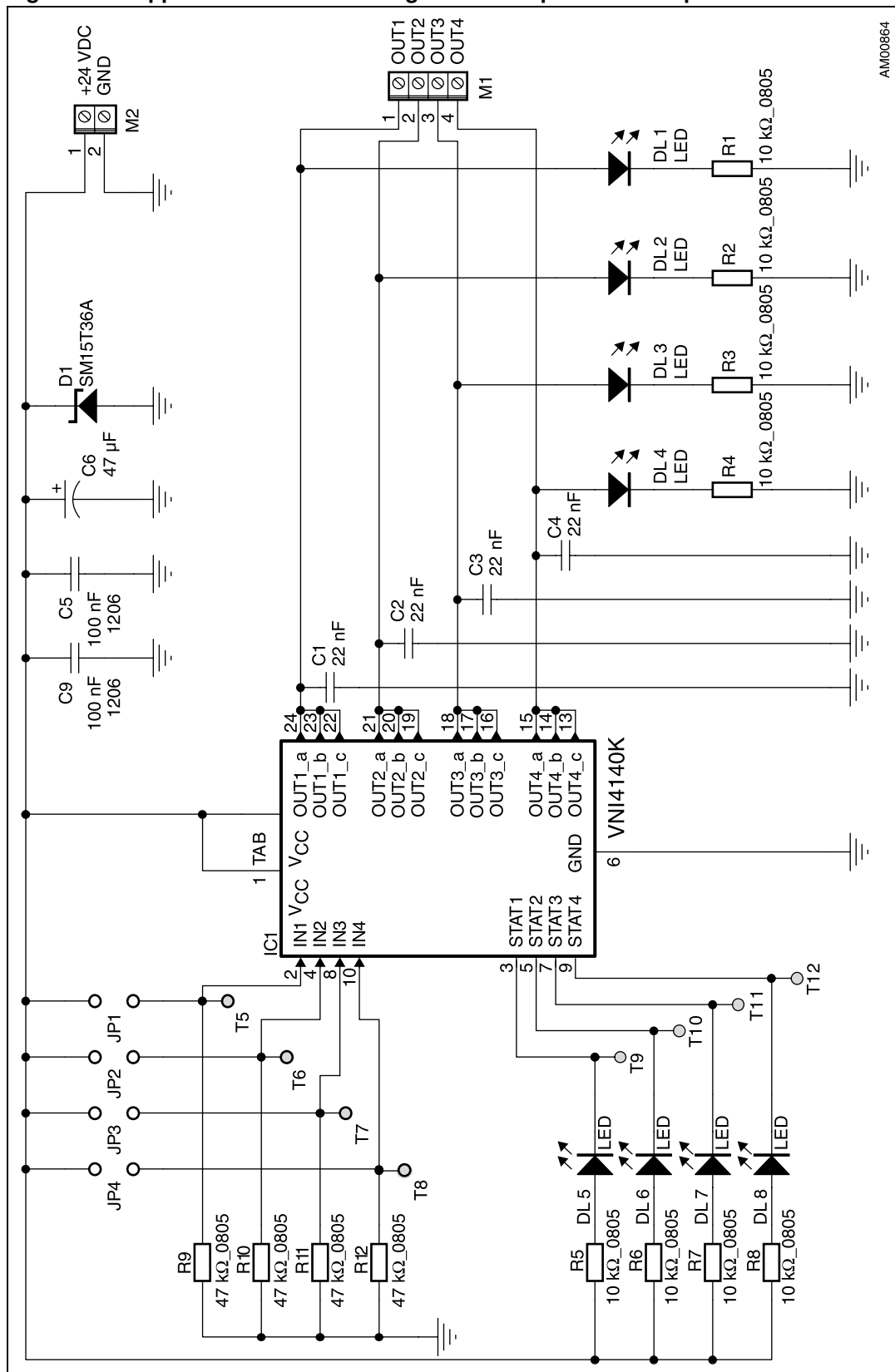
## 3 Application solutions

Ideas (application environment) on how to optimize the immunity of the device are listed in [Section 3.1](#), [Section 3.2](#) and [Section 3.3](#).

### 3.1 Cap filters

This basic configuration uses 22 nF ceramic capacitors connected between the device outputs and ground. It protects the VNI4140K primarily against radio-frequency and fast transient disturbances.

Figure 3. Application schematic diagram with capacitive filter protection



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With this basic configuration, application immunity is limited in the case of a negative ESD pulse of -8 kV (air discharge), as listed in [Table 1](#).

**Table 1. Application immunity with C filters**

| Test signal level [kV] | Polarity / result criteria |   |
|------------------------|----------------------------|---|
|                        | +                          | - |
| 2                      | B                          | B |
| 4                      | B                          | B |
| 6                      | B                          | B |
| 8                      | B                          | D |
| 10                     | B                          | D |
| 12                     | B                          | D |

### 3.2 II filters

Improved results are achieved when using II LC filters at the VNI4140K outputs. Measurements show the best results with 22 nF ceramic capacitors and approximately 82 nH inductors. The inductor can be implemented either as a “spiral” directly on the PCB substrate, or placed as a discrete component.

If, based on available space, the inductor is implemented as a “spiral” directly on the PCB substrate, the cost of a discrete conductor is saved. An example is shown in [Figure 4](#).

The discrete inductor should be a wire-wound, air-core type if possible. Ferrite-based inductors did not produce positive results. An example of a suitable component is the 1812SMS-82NJLB, Midi Spring® Air Core inductor from Coilcraft.

**Figure 4. Example of a spiral PCB inductor**

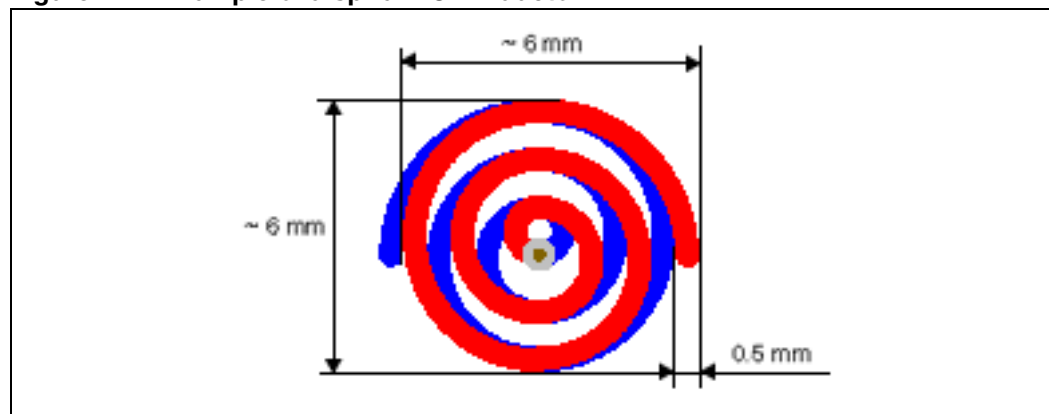




Figure 5. Midi Spring inductors

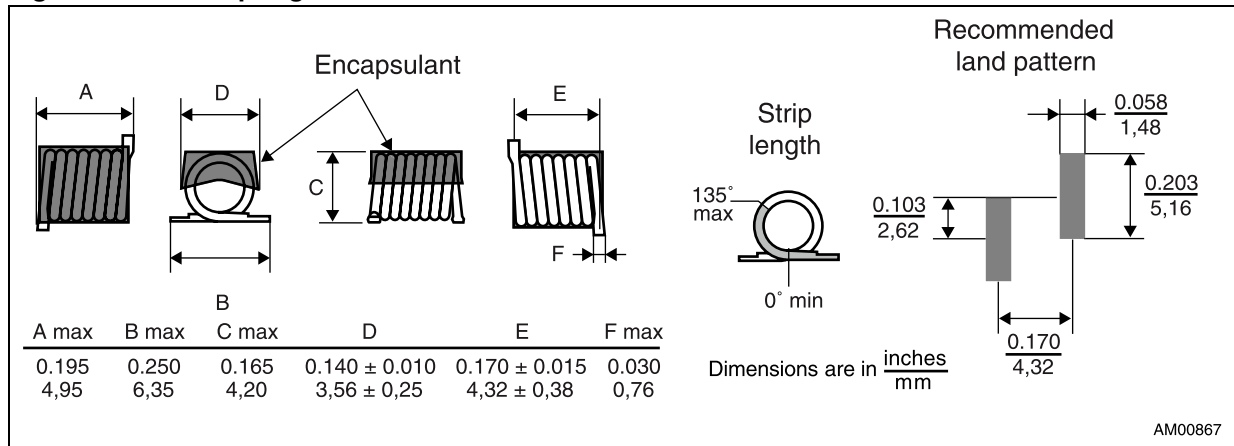
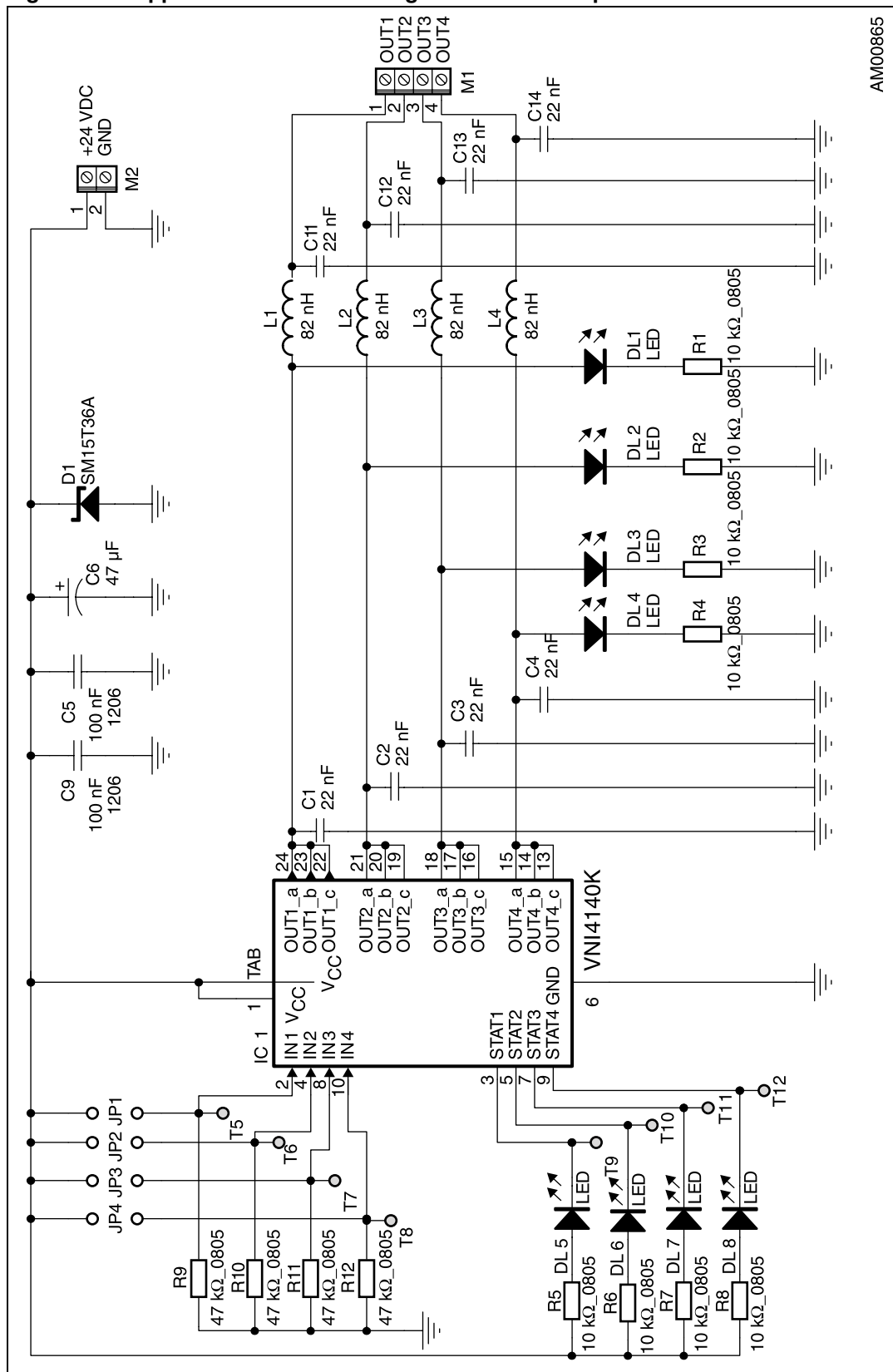


Figure 6. Application schematic diagram with  $\Pi$  filter protection



The results in [Table 2](#) are achieved employing  $\Pi$  LC filters. This configuration appears to be a satisfactory compromise between the PCB space occupied, component cost and application immunity, which is notably improved. In this case, the application withstands air discharges up to -14 kV without silicon degradation or damage (using the Midi Spring inductors).

**Table 2. Application immunity with  $\Pi$  filters**

| Test signal level [kV] | Polarity / result criteria <sup>(1)</sup> |                      |
|------------------------|---|----------------------|
|                        | $\Pi$ (LC) filter                         |                      |
|                        | +   | -                    |
| 8                      | B   | B                    |
| 10                     | B   | B                    |
| 12                     | B   | B                    |
| 14                     | B   | B / D <sup>(2)</sup> |
| 15                     | B   | D                    |
| 16                     | B   | —                    |

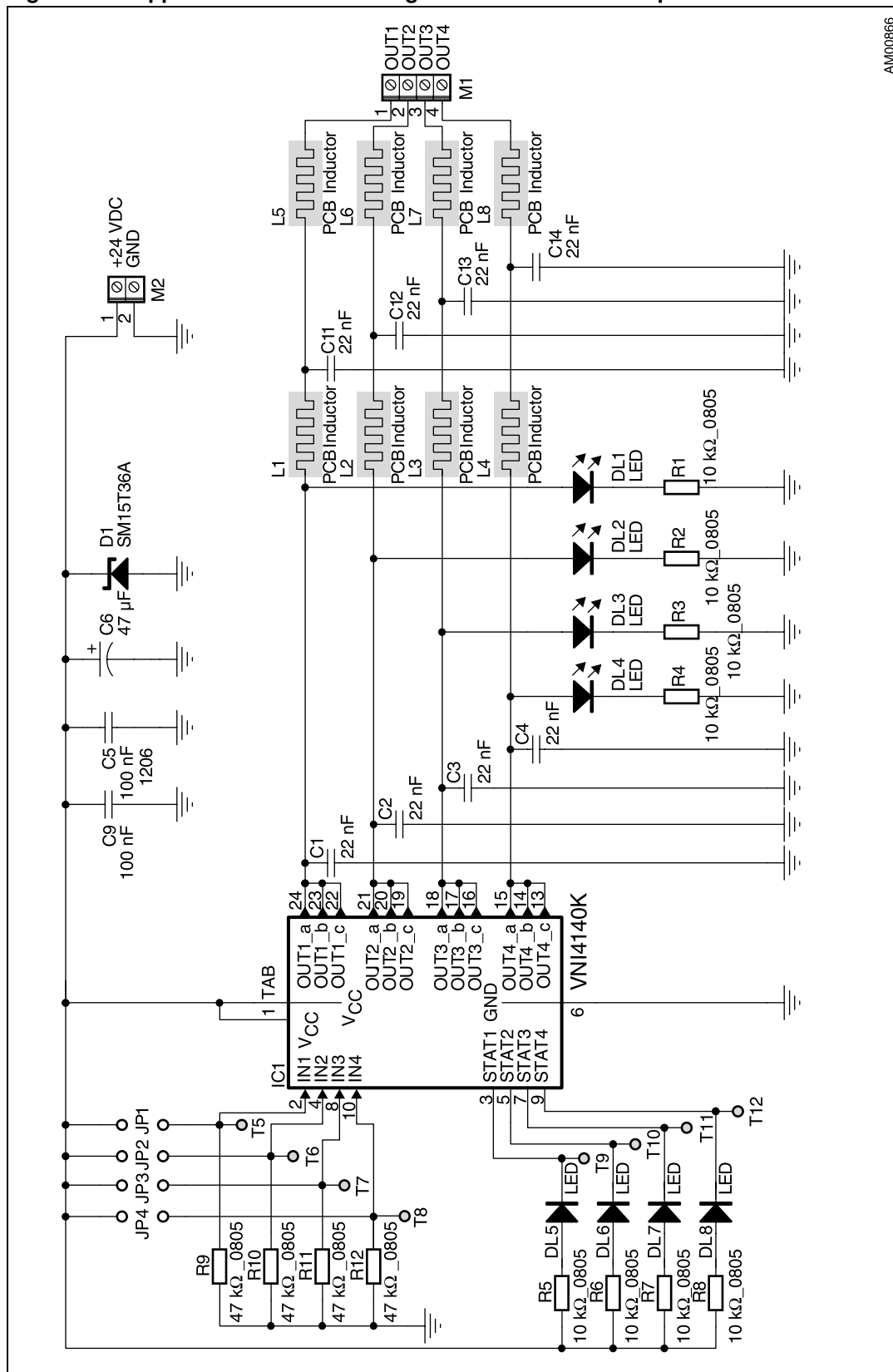
1. The results shown are based on testing with Midi Spring inductors.

2. Based on testing with PCB inductors.

### 3.3 Dual LC filters

The best performance is achieved using dual (cascade) LC filters. The schematic diagram and test results are provided in [Figure 7](#) and [Table 3](#).

Figure 7. Application schematic diagram with dual LC filter protection



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Figure 8. Test board views

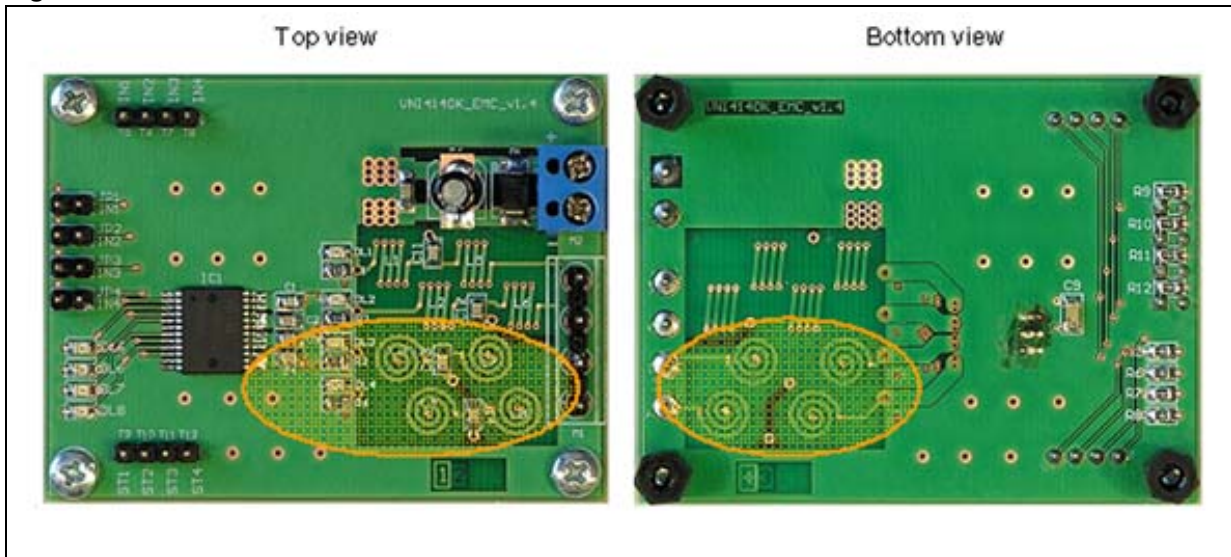


Table 3. Application immunity with dual LC filters

| Test signal level [kV] | Polarity / result criteria <sup>(1)</sup> |   |
|------------------------|---|---|
|                        | +   | - |
| 8                      | B   | B |
| 10                     | B   | B |
| 12                     | B   | B |
| 14                     | B   | B |
| 15                     | B   | B |
| 16                     | B   | D |

1. Tests performed with "spiral" PCB inductors.

An increase in immunity of approximately 3 kV can be observed compared to the  $\Pi$  filter configuration (with PCB inductor). Whether or not to use the dual filter is based on application requirements.

## 4 Conclusion

The VNI4140K application is immune to the positive polarity of the ESD at a voltage level higher than 16 kV.

In the case of negative pulse immunity, special attention should be paid to the output filter, which slows down the ESD pulse. Three configurations have been tested.

The dual LC filter (cascade connection) structure is highly immune but requires more space on the PCB. A level of -15 kV without silicon degradation was achieved.

The configuration using  $\Pi$  filters provides a good compromise between the immunity and PCB space in this implementation. A level of -14 kV (using Midi Spring inductors) / -12 kV (PCB inductors) without silicon degradation was achieved.

The basic device connection with a single ceramic capacitor at each output provides robustness against -6 kV ESD pulses.

## 5 References

1. VNI4140K device datasheet
2. AN2684 - STEVAL-IFP006V1: designing with VNI4140K quad high-side smart power solid-state relay ICs
3. AN2208 - Designing Industrial Applications with VN808/VN340SP High-side Drivers
4. AN1351 - VIPower AND BCDmultipower: making life easier with ST's high side drivers
5. IEC61000-4-2 Electrostatic discharge

## 6 Revision history

Table 4. Document revision history

| Date        | Revision | Changes          |
|-------------|----------|------------------|
| 24-Mar-2010 | 1        | Initial release. |



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